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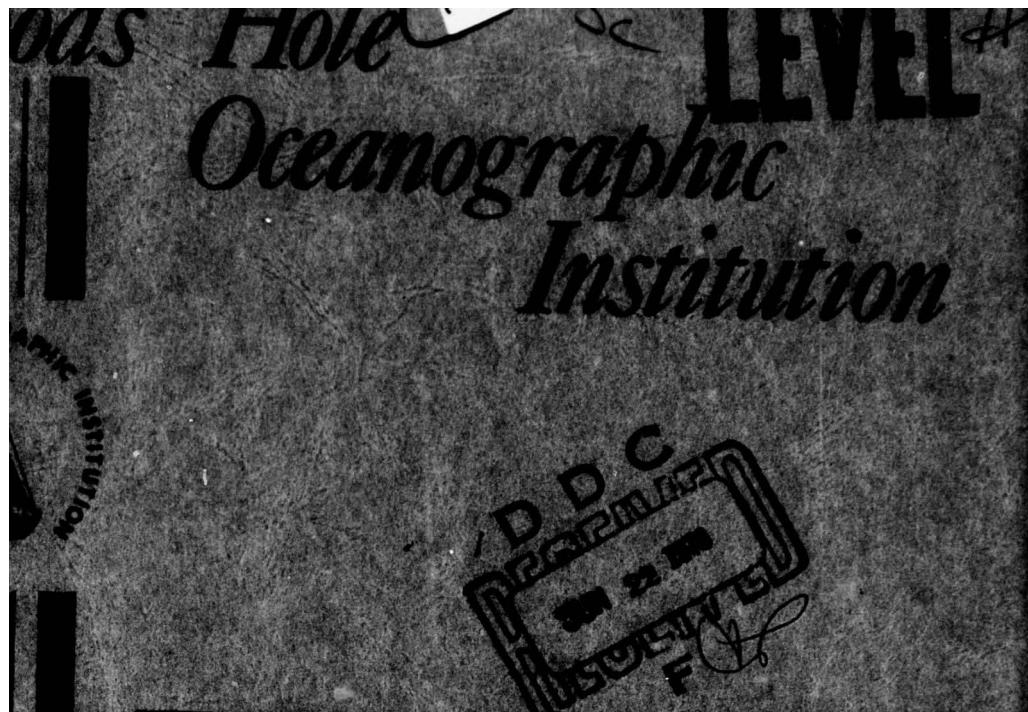
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A COMPILATION OF MOORED CURRENT DATA  
AND ASSOCIATED OBSERVATIONS  
(MOOE-SITE, VOL. XVI, 1971-1975)

by

Susan Tarbell  
and  
Ann Spencer

March 1978

TECHNICAL REPORT

Prepared for the Office of Naval Research  
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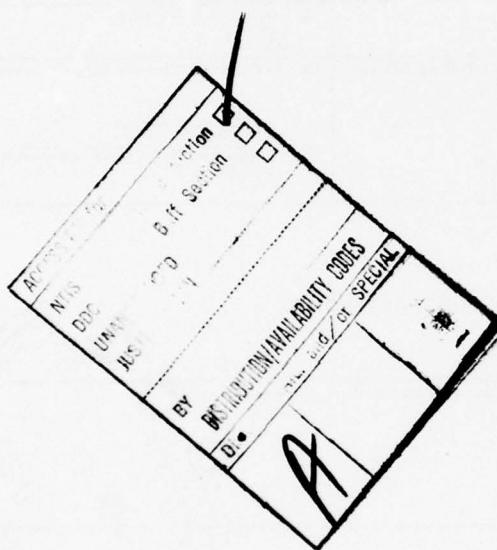
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→ spatial or temporal array. Selected CTD data are included and displayed as potential temperature and salinity versus pressure.



WHOI-78-5

A COMPILATION OF MOORED CURRENT DATA AND ASSOCIATED  
OBSERVATIONS (MODE-SITE, VOL. XVI 1971-1975)

By

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WOODS HOLE OCEANOGRAPHIC INSTITUTION  
Woods Hole, Massachusetts 02543

March 1978

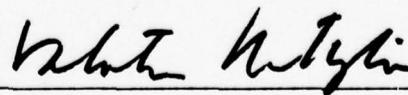
TECHNICAL REPORT

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L. Valentine Worthington, Chairman  
Department of Physical Oceanography

#### ABSTRACT

Current, temperature and pressure measurements from instruments moored in the MODE area during the years 1971-1975 are presented. Record lengths vary from 2 weeks to 7 months. Data from individual instruments are displayed in the form of statistical tables, spectral plots and variables vs. time plots. Current data are additionally displayed as progressive vector plots. Composite plots of temperature, pressure or velocity are included for groups of records which could be combined to show a meaningful spatial or temporal array. Selected CTD data are included and displayed as potential temperature and salinity versus pressure.

PREFACE

This volume is the sixteenth of a series of data reports presenting moored current meter and associated data collected by the W.H.O.I. Buoy Group.

Volumes I through XV present data from the years 1963-1971, and from several special experiments: the 1970 Pollard array, the 1973 IWEX array, the 1973 MODE array, and the Saint Croix mooring measurements.

Volume XVI presents MODE region data from 1971 through 1975.

Volume *	W.H.O.I.*		* Notes
Number *	Ref. # *		*year experiment
*****			
I	65-44	Webster, F., and N. P. Fofonoff	
II	66-60	Webster, F., and N. P. Fofonoff	
III	67-66	Webster, F., and N. P. Fofonoff	
IV	70-40	Pollard, R. T.	
V	71-50	Tarbell, S., and F. Webster	1966 measurements
VI	74-4	Tarbell, S.	1967 measurements
VII	74-52	Chausse, D., and S. Tarbell	1968 measurements
VIII	75-7	Pollard, R. T., and S. Tarbell	1970 Array data
IX	75-68	Tarbell, S., M. G. Briscoe, and D. Chausse	1973 IWEX Array
X	76-40	Tarbell, S.	1969a measurements
XI	76-41	Tarbell, S.	1969b measurements
XII	76-101	Chausse, D., and S. Tarbell	1973 MODE Array
XIII	77-18	Tarbell, S., and A. W. Whitlatch	1970 measurements
XIV	77-41	Tarbell, S., R. Payne, and R. Walden	1976 Mooring 592, Saint Croix
XV	77-56	Tarbell, S., and A. W. Whitlatch	1971 measurements

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#### ACKNOWLEDGMENTS

Data return from moored instruments improved markedly over the years covered in this report. Acknowledgments should go to the buoy engineers and operations personnel who solved numerous problems and introduced many innovative techniques. Together with the crews of the R/V Chain, the R/V Knorr and the R/V Atlantis II, they developed increasingly more reliable procedures for mooring deployment and recovery.

The current meter data in this report were processed with the help of all members of the data processing group under the guidance of the scientific staff. The CTD data were processed by N. Pennington and prepared for publication by C. Mills.

The following agencies are acknowledged for their support of the experiments and data preparation which form the basis of this report: the National Science Foundation (IDOE contract numbers GX29054, OCE 75-03962) and the Office of Naval Research (contract numbers N00014-66-C0241 NR083-004, N00014-74-C0262 NR083-004

Presentation

This report is shown in its entirety on microfiche with a summary presented on printed pages for easier access. The summary gives a general description of the MODE area moorings, some details of the instrumentation used in acquiring the data and a description of the computer display programs. It also contains composite plots of filtered current, temperature and pressure data.

The first page of microfiche contains the summary and selected CTD plots. The CTD plots are shown only on microfiche. The seven rows of the first microfiche page are organized as follows:

Row A Text

Row B Text

Row C Composite plots by mooring location

Row D Composite horizontal array plots

Row E Composite temperatures from T/Ps

Row F Composite pressures from T/Ps

Row G Plots of temperature and salinity from CTD lowerings

The basic current meter displays are organized on subsequent microfiche sheets so that the displays for an individual instrument are arranged down a microfiche column, and similar plots for different instruments are arranged across the rows.

The seven rows of data displays on microfiche are as follows:

Row A Mooring diagrams

Row B Data identifier

Row C Instrument information and computed statistical quantities

Row D Spectral diagrams

Row E Progressive vector plots

Row F u and v plotted against time

Row G Speed, direction (and temperature if available) plotted against time

On microfiche #6, the last 3 columns have a different format due to the length of the time series.

No data are presented for the various tensiometers and inclinometers set on some moorings, nor for experimental depth or temperature recorders.

## Introduction

The data presented in this report are from the MODE region here defined to be a circular area of about 1000 square kilometers centered on 28°N, 69° 40'W (see Fig. 1). The records span 3½ years from 1971 to 1975.

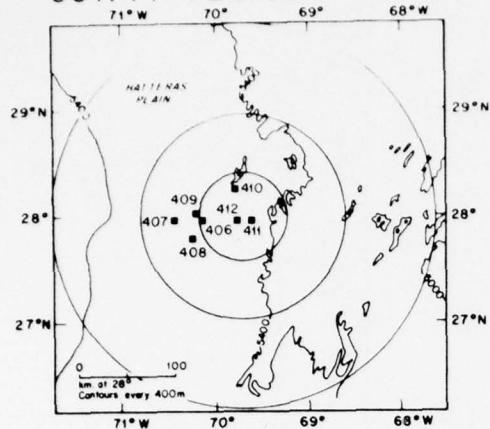
The first array (MODE-0, Array 1) consisted of two surface and five intermediate moorings located around and to the west of MODE-Center, (28°N, 69° 40'W) where the bottom topography was smooth. The second array consisted of four intermediate, 1 surface and a deep mooring, located east of MODE-Center where the bottom topography was rough. The third array was more widely spaced, and consisted of four surface moorings, one with a wind recorder, and one intermediate mooring. The fourth array consisted of two intermediate moorings at MODE-Center and MODE-East (28°N, 68° 40'W). The fifth array (Chausse, Tarbell, 1976) was set as part of the MODE-I experiment.

The arrays set after MODE-I are referred to as site moorings. Their locations were at MODE-Center (28°N, 69° 40'W) and MODE-East (28°N, 68° 40'W) and intermediate moorings were used throughout.

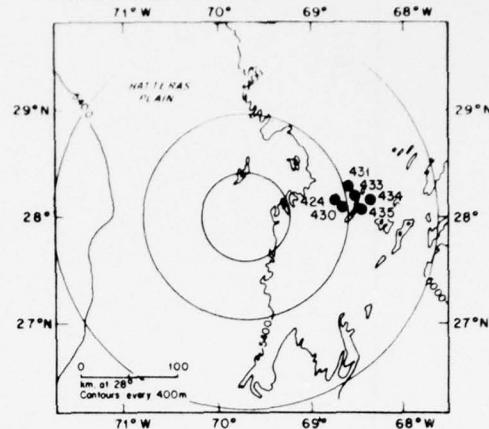
Details of mooring locations and durations at sea are presented in Figures 1, 2 and Table 1.

The first three MODE-0 arrays were deployed to find an optimum design for the MODE-I experiment (Heinmiller, 1975). They were in different locations, of different spatial density and of different mooring types. The fourth array and the post-MODE site moorings were deployed to obtain long-term records for study of low frequency phenomenon (Schmitz, 1977). Mooring 542 was set as part of a subsequent experiment and was also a continuation of the moorings set at MODE-Center. It is included in this report to show the full extent of the data gathered at that location.

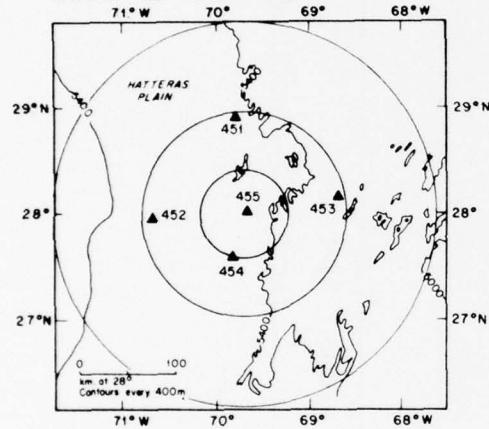
MODE O ARRAY 1  
OCT. 71-FEB. 72



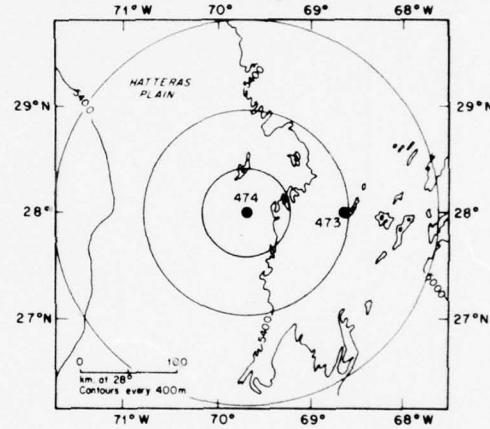
MODE O ARRAY 2  
FEB. 72-MAY. 72



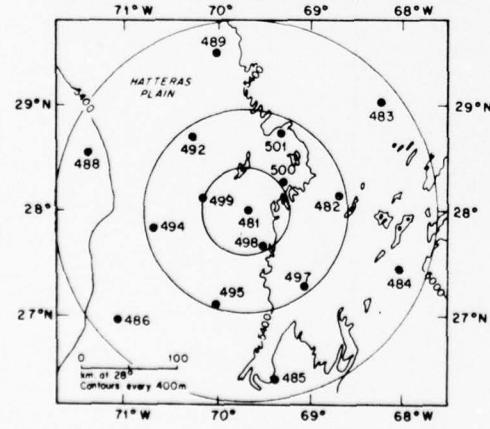
MODE O ARRAY 3  
MAY. 72-OCT. 72



SITE MOORINGS  
OCT. 72-MARCH 73



MODE 1 ARRAY  
MARCH 73-JUNE 73



SITE MOORINGS  
JUNE 73-APRIL 75

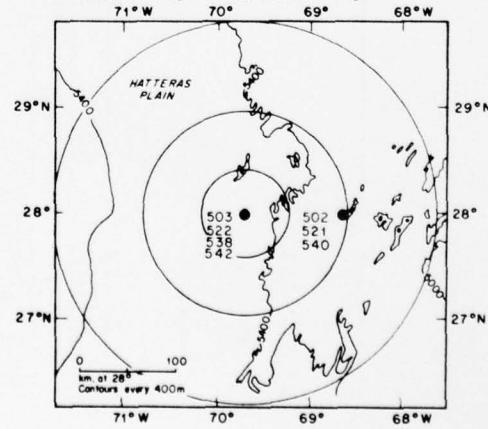


FIGURE 1 MOORING POSITIONS

FIGURE 2

DURATION OF MOORINGS

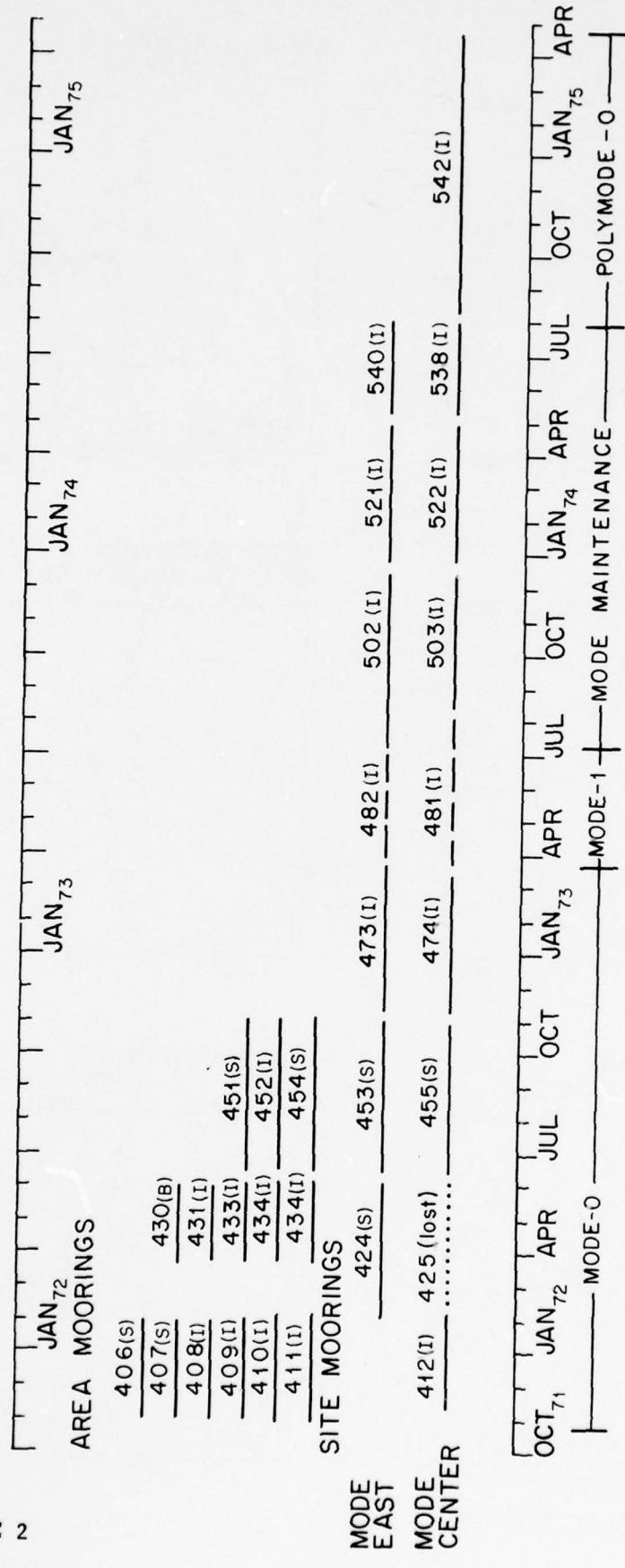


Table 1  
Summary of MODE 0 and MODE Site Moorings

Mooring Number	Type *	Location (lat. N., long. W)		Bottom Depth (m)	Set, Retrieval Dates
	S I IW B				
<b>Array 1</b>					
406	S	27°59.8'	70° 0.3'	5460	Oct. 29'71-Feb. 7'72
407	S	28° 0.4'	70°20.6'	5465	Oct. 30'71-Feb. 9'72
408	I	27°49.0'	70° 8.8'	5470	Oct. 30'71-Feb. 9'72
409	I	28° 1.5'	70° 6.8'	5465	Oct. 30'71-Feb. 9'72
410	I	28°21.5'	69°41.5'	5460	Oct. 31'71-Feb. 9'72
411	I	28° 0.7'	69°31.3'	5427	Oct. 31'71-Feb. 7'72
412	I	28° 0.2'	69°41.5'	5455	Oct. 31'71-Feb. 7'72
<b>Array 2</b>					
424	S	28° 9.1	68°36.8'	5254	Feb. 6'72-May 25'72
425	S	28° 0.8'	69°39.8'	5462	Feb. 8'72-Lost-
430	B	28° 9.8'	68°34.5'	5221	Mar. 18'72-May 25'72
431	I	28°20.3'	68°24.8'	5370	Mar. 19'72-May 26'72
432	I	28°10.5'	68°23.8'	5380	Mar. 20'72-Aborted
433	I	28°10.5'	68°23.8'	5380	Mar. 20'72-May 27'72
434	I	28°10.2'	68°11.8'	5275	Mar. 20'72-May 26'72
435	I	27°58.7'	68°24.7'	5280	Mar. 21'72-May 26'72
<b>Array 3</b>					
451	S	28°54.4'	69°41.0'	5437	May 23'72-Nov. 1'72
452	I	27°59.8'	70°38.7'	5452	May 23'72-Oct. 31'72
453	S	28°10.1'	68°38.2'	5261	May 25'72-Oct. 30'72
454	S	27°33.7'	69°41.8'	5462	May 28'72-Oct. 31'72
455	S	28° 0.6'	69°37.6'	5462	May 28'72-Nov. 4'72
<b>Site Mooring</b>					
473	I	28°10.7'	68°36.1'	5261	Oct. 30'72-Mar. 11'73
474	I	28° 1.4'	69°39.4'	5462	Nov. 4'72-Mar. 10'73
<b>Site Mooring</b>					
502	I	28° 8.9'	68°41.4'	5255	June 26'73-Dec 13'73
503	I	28° 0.2'	69°44.4'	5461	June 27'73-Dec 14'73
521	I	28° 9.5'	68°41.5'	5265	Dec. 13'73-Apr 20'74
522	I	28° 0.5'	69°44.8'	5462	Dec. 14'73-Apr 21'74
538	IW	28° 2.6'	69°44.8'	5457	Apr. 18'74-Jul 27'74
540	I	28° 8.9'	68°40.4'	5265	Apr. 20'74-Jul 29'74
542	IW	28° 1.4'	69°38.9'	5462	July 27'74-Apr 26'75

\* S = Surface compound mooring

I = Intermediate compound mooring

IW = Intermediate all wire mooring

B = Bottom mooring

### Moorings

Both surface and intermediate moorings were set in the early 1970s. (See Table 1.) Growing evidence that current meter data were contaminated by noise from surface waves propagating down the mooring line led to the increasing use of intermediate moorings. The compound intermediate mooring (Heinmiller, 1976) proved extremely reliable with only 3 failures in 103 moorings. In the MODE-1 experiment there were large discrepancies between the intended and actual instrument depths (Chausse and Tarbell, 1976), which were due in part to the unpredictable stretch factor of the Dacron line. In 1974, the first all-wire intermediate moorings (538, 542) were set in an effort to maintain the instrumentation at its intended depth.

Numerous minor improvements were made over the years to increase the reliability of various mooring components. For instance, glass spheres were placed in plastic hard hats instead of nets to reduce the risk of an implosion severing the mooring line. Such changes enabled moorings to be set with confidence for 9 months or longer as scientific necessity dictated.

For greater detail about MODE area moorings, see Heinmiller (1975), Heinmiller (1976) and Berteaux and Heinmiller (1973).

### Current Meter Types

The current meters described in this report were either Vector Averaging Current Meters (VACMs), built by American Machine and Foundry (AMF) or Model 850 current meters built by Geodyne, now a part of Egerton, Germeshausen and Grier (EG&G).

The Model 850 current meter stores burst sampled data on magnetic tape cartridges. Each Model 850 collected and stored 23 (or 24) data cycles which were sampled every 5.27 seconds. The instrument then turned off for the remainder of the recording interval, usually either 15 or 30 minutes. Those Model 850s which were modified to include temperature measurements accumulated the count from the temperature circuit from one 5.19 second period and stored it at the beginning of each data burst.

The VACM stores variables on 1/8" magnetic tape cassettes at the end of each recording interval, typically every 30 minutes. Values in the East and North register are computed from compass, vane and rotor values each time a rotor magnet passes the sensing diode. The velocity components are accumulated over the recording interval resulting in vector averaged velocities. The temperature count is summed from the pulses of a voltage to frequency converter, whose output frequency is relayed to the thermistor resistance at its input (Payne et al., 1976).

#### Temperature/Pressure Recorder

An instrument to measure and store temperature, pressure and time data (T/P) was developed in the Draper Laboratory at M.I.T. for the MODE-1 Data Array, and used extensively on the post-MODE moorings. The instrument stores a data sample every 15 seconds and records the sum of 64 successive data samples on a magnetic tape cassette every 16 minutes ( $64 \times 15 = 960$  seconds = 16 minutes).

The time base generator, a crystal oscillator, has an accuracy of  $\pm 1$  second per day.

The temperature has an accuracy of about  $.01^{\circ}\text{C}$  and a resolution of  $.001^{\circ}\text{C}$  (Wunsch and Dahlen, 1974).

The pressure sensor is a strain gauge with a manufacturer specified accuracy of .03% of the scale range used (Wunsch and Dahlen, 1974).

#### CTD

The CTDs were constructed at W.H.O.I. by Neil Brown (Brown, 1974; Fofonoff, Hayes and Millard, 1975; Brown and Morrison, 1978). The instruments measure conductivity, temperature and pressure. Plots of potential temperature and salinity versus pressure are included on the first page of microfiche.

Time

A time base for the T/Ps, 850s and VACMs is set by a quartz crystal oscillator with a manufacturer's specified accuracy of  $\pm 1$  second per day.

To provide secondary time information for current meter records, artificial events are placed in the rotor field both before and after the sea data. The procedure for this is as follows:

For First Events:

- Step 1. Turn the recording circuit on (not to be turned off until recovery).
- Step 2.
  - a) Block the rotor to prevent it from turning.
  - b) Allow the instrument to record several data cycles with the rotor immobilized.
- Step 3. (t) Ten seconds after a recording interval starts, spin the rotor as fast as possible.
- Step 4. (t) In a successive record spin the rotor again.
- Step 5. Block rotor again until just before launch.
- Step 6. (t) Free the rotor at launch.

For Last Events:

- Step 1. (t) After recovery, block rotor for several recording intervals.
- Step 2. (t) Ten seconds after a recording interval starts, spin the rotor.
- Step 3. (t) Spin the rotor again in a subsequent record.
- Step 4. Block the rotor for several records before shutting off the record circuit.

The steps that are marked with a (t) are the most easily seen in the data and times should be noted using a radio time signal e.g., WWV or CHU.

Under normal operating conditions the elapsed time measured by the clock word matches the real elapsed time.

In this report time is read as year-month-day hour.minute.second.

### Current Meter Data Processing

Bit strings from magnetic tapes for Model 850s (1/4" 2-track cartridges) and VACMs (1/8" 4-track cassettes) were transcribed onto 9-track computer compatible tape at W.H.O.I. The data were then converted to scientific units (decoded) and stored on magnetic tape in Maltais format (Maltais, 1969).

Editing the data included selecting times for the beginning and ending of each record, adjusting the nominal depth of some records to agree with information supplied by the T/Ps, applying corrections to temperature indicated by post cruise thermistor calibrations, computing vector averaged components for the data from burst sampled Model 850 instruments, and interpolating through gaps in the data caused by the removal of erroneous records.

The result is an evenly spaced time series which is used as a basic input for all further processing.

The current data were classified into three categories (good, questionable and bad). "Good" is defined to mean that all sensors worked properly. "Questionable" means that the data has a known problem which might not affect the low frequency data, e.g., 5032. "Bad" means that at least one of the sensors did not work at all. The individual data series presented in this report contain mostly "Good" and some "Questionable" data. Questionable data is indicated on the Instrument page (row C on the microfiche pages presenting data).

Table 2 indicates which variables are presented with reference to mooring numbers and approximate depths.

Data Identifiers

To insure that each data series has a unique identifier, the following guide lines are used; 538,10B900

- 538 - The first three digits are the mooring number
- ,10 - The 10th instrument down the mooring line. A one digit mooring position is not preceded by a comma (5385D900).
- B - The position of the letter in the alphabet indicates the amount of editing that has been done. The symbol \$ means no editing has been done.
- 900 - Vector averaging interval (in seconds). 1H would mean 1 hour averages, 1D for 1 day averages.
- 1DGAU24 - A 1 day averaged series from Gaussian filtered data, the filter having a half width of 24 hours.

Table 3, which has the same format as Table 2 indicates the position number, depth and type of each instrument which has data in this report.

Pre MODE Data Series - MODE 0																		
	Array 1					Array 2					Array 3							
0	406	407	408	409	410	411	412	424	430	431	433	434	435	451	452	453	454	455
500	V	V												VT	VT	VT	VT	
800	V																	
1500	VT	VT	V	VT	V	V	VT	VT							VT		VT	
1600	V																	
4000	V	V		V	V			VT	VT	V	V	V	T		PT	T		
4200	V													V	V	V	V	
5000+								VT	V									
Post MODE Data Series - Site Moorings																		
	473	474	502	503	521	522	538	540	542									
500			V	V	V	V	V	V	VT	V	VT							
600									TP	TP	TP	TP						
800									TP		TP	TP	TP					
1000									TP		TP	TP	TP					
1500			V	V	V	V	V	V	VT	V	VT							
2000									TP	TP	TP	TP						
2500									TP	TP	TP	TP						
3500									TP	TP	TP		TP					
4000			V	V	V			V	V	VT	V	V		TP				
4500									TP	TP	TP	TP						
5000+									TP	TP	TP	TP						

TABLE 2 VARIABLES PRESENTED V=VELOCITIES  
T=TEMPERATURES  
P=PRESSURE

Instrument Depth and Data Identifier Summary

Meters	Pre MODE - MODE 0								Post MODE - Site Moorings									
	Array 1				Array 2				Array 3									
	406	407	408	409	410	411	412	424	430	431	433	434	435	451	452	453	454	455
0														0				
500	514	514												515	561	514		514
	(3)	(1)												(2)	(2)	(2)		(2)
800	816																	
	(4)																	
1500	1518	1516	1503	1522	1504	1476	1502	1519							1516		1516	
	(5)	(2)	(1)	(1)	(1)	(1)	(1)	(2)							(3)		(3)	
1600	1620																	
	(6)																	
4000	4003	4001		4028	4008			4074	3975	3955	3990	3970	3968			3970		
	(7)	(3)		(2)	(2)			(3)	(1)	(2)	(2)	(2)	(4)			-5-		
																4075		
																(6)		
4200	4202													4191	4181		4207	4208
	(8)													(3)	(6)	(4)	(4)	
5000+								5131	5119									
								(4)	(2)									
Water																		
Depth (m)	5460	5465	5470	5465	5460	5427	5455	5254	5221	5370	5380	5275	5280	5437	5452	5261	5462	5462

TABLE 3 DEPTHS OF INDIVIDUAL INSTRUMENTS IN

METERS

INSTRUMENT POSITION NUMBER AND

INSTRUMENT TYPE; (N) for CM, -N- for

T/P

### Computer Programs

The following programs have been used to generate the data displays in this report:

#### *Statistics (STATS)*

Standard statistical parameters are calculated for data in the time range given at the bottom of the table. Given  $n$  speed and direction or temperature values in a sample, we define  $E_i = S_i \sin \theta_i$ ,  $N_i = S_i \cos \theta_i$ , then for  $A = E, N, S$ , and  $T$ ,

$$\text{mean, } \bar{A} = \frac{1}{n} \sum_{i=1}^n A_i \quad \text{variance, } \sigma_A^2 = \frac{1}{n} \sum_{i=1}^n A_i^2 - \bar{A}^2$$

$$\text{standard error of the mean} = \frac{\sigma_A}{\sqrt{n}} \quad \text{standard deviation} = \sigma_A$$

$$\text{skewness} = \frac{1}{\sigma_A^3} \left[ \frac{1}{n} \sum_{i=1}^n A_i^3 - \frac{3\bar{A}}{n} \sum_{i=1}^n A_i^2 + 2\bar{A}^3 \right]$$

$$\text{kurtosis} = \frac{1}{\sigma_A^4} \left[ \frac{1}{n} \sum_{i=1}^n A_i^4 - \frac{4\bar{A}}{n} \sum_{i=1}^n A_i^3 + \frac{6\bar{A}^2}{n} \sum_{i=1}^n A_i^2 - 3\bar{A}^4 \right]$$

Note that the kurtosis becomes unstable for sufficiently narrow distributions (see record 521,12).

The program also calculates "East and North" statistics,

$$\text{covariance, } M = \frac{1}{n} \sum_{i=1}^n E_i N_i - \bar{E} \bar{N}$$

$$\text{standard deviation of covariance, } \sigma_M = \sqrt{\frac{1}{n} \sum_{i=1}^n (E_i N_i)^2 - \bar{E} \bar{N}^2}$$

$$\text{standard error of covariance} = \frac{\sigma_M}{\sqrt{n}}$$

$$\text{correlation coefficient, } M' = \frac{M}{\sigma_E \sigma_M} .$$

The program also calculates parameters related to vector quantities:

the scalar amplitude of the vector mean,  $V_m = \sqrt{E^2 + N^2}$ ; vector variance

$$V_v = \frac{1}{2} (\sigma_E^2 + \sigma_N^2); \text{ standard deviation} = \sqrt{V_v} .$$

#### *Progressive Vector Diagram (PROVEC)*

The progressive vector displacements are plotted. The plot begins with an asterisk (\*) on a day boundary. All following interval boundaries are indicated by a symbol, which changes with each month in the case of longer records. This type of plot accentuates very low frequency events at the expense of higher frequency oscillations.

#### *Variable vs. Time Plot*

This is a diagram of any variable plotted as a function of TIME. The plot is generated from the 1-hour averaged series. This type of plot is complementary to the progressive vector diagram since it accentuates higher frequency events such as inertial and tidal oscillations.

#### *Spectra*

The program TIMSAN (TIme Series ANalysis) uses the Fast Fourier Transform algorithm of Singleton (1969) and is restricted to data segments of length  $N$  points, where  $N$  must be an even number which has no prime factor larger than 5, and must be less than 8000 points; data series longer than this must be broken into two or more pieces.

The number of degrees of freedom for the first 40 plotted points is given by  $v = a m s$  where  $m$  is the number of adjacent frequency bands being averaged as stated in the label,  $s$  is the number of independent data pieces being averaged, again as stated in the label, and  $a$  should be set equal to 2 for temperature spectra and for Horizontal Kinetic Energy (HKE) spectra for which the EAST and NORTH components seem statistically independent. In the absence of information regarding NORTH-EAST correlation, one should use  $a = 2$  to be safe.

The log-log plot is further averaged during plotting so that more and more points are averaged together as frequency increases. This eliminates the bunching together of points at high frequencies, increases the degrees of freedom of the high frequency estimates, and still permits low-frequency resolution. The averaging algorithm is as follows: counting from the left of the plot, the first 40 plotted points represent data that has been averaged as stated in the label; the data for the next 15 plotted points has been averaged over twice as many frequency bands; the next 6 over five times as many, the next 40 over ten times as many, the next 15 over twenty times as many, the next 6 over fifty times as many, the next 40 over 100 times as many and so on. In this way, for example, 7900 data points with no averaging indicated in the label would be plotted as only 176 points, and the last 14 estimates would be averaged over 200 basic frequency bands. The  $m$  in the formula  $v = a m s$  for degrees of freedom is, in this example, 200 times larger at the highest frequencies than at the lowest frequencies.

For  $v \geq 30$ , the confidence limits for the spectral estimates are given approximately by  $(1 - 2/9v \pm Z\sqrt{2/9v})^3$  where  $Z = 1.28375$  for 80% confidence limits,  $Z = 1.645$  for 90%,  $Z = 1.96$  for 95% and  $Z = 2.5757$  for 99%. In the example above, if the HKE spectral plot label had indicated 2 pieces and averaging over 8 adjacent frequency bands then  $v = 2 \times 2 \times 8 = 32$  for the lowest frequencies (assuming NORTH and EAST components are highly correlated) and  $200 \times 32 = 6400$  for the highest frequencies. The 95% confidence intervals (i.e., 95% of the time one would expect the spectral estimates to vary no more than this much) would be (0.57, 1.55) at low frequencies, and (0.97, 1.03) at high frequencies.

For  $v \leq 30$ , one must obtain confidence intervals from Chi-Squared distribution tables in standard statistical references.

Temperature spectra from 850 current meters show aliasing at high frequencies because of the sampling scheme. Speed and direction are burst sampled within each recording interval. These samples are vector averaged to attenuate high frequency aliasing in the current measurement. There is only one 5.19 second temperature sample per recording interval, however. The temperature spectrum for data series shows clearly the resulting high frequency aliasing. In contrast, the VACM averages all variables over the full recording interval, virtually eliminating the problem.

### *Gaussian Filtered Plots*

The basic time series is filtered using a symmetrical running Gaussian filter with a half width of 24 hours. The filtering is sequential and the resultant time series is 48 hours shorter than the input time series (the first and last 24 hours are lost), and the sampling interval is the same. A simple running hat filter is then applied to the series to form a series with one data point per day, the point being the average for each day measured from midnight to midnight.

#### *A) Vector Stick Plots*

The filtered velocity vectors are plotted along a time scale. Unless otherwise indicated, the vector orientation is such that north is up. The length of the "stick" is proportional to speed.

#### *B) Line Plots*

Pressure and temperature are filtered as described above, and one point per day is plotted along a time scale.

#### *C) Sequential Array Plots*

Subsampled filtered velocity vectors or temperature values are plotted to show a spatial array at a particular depth.

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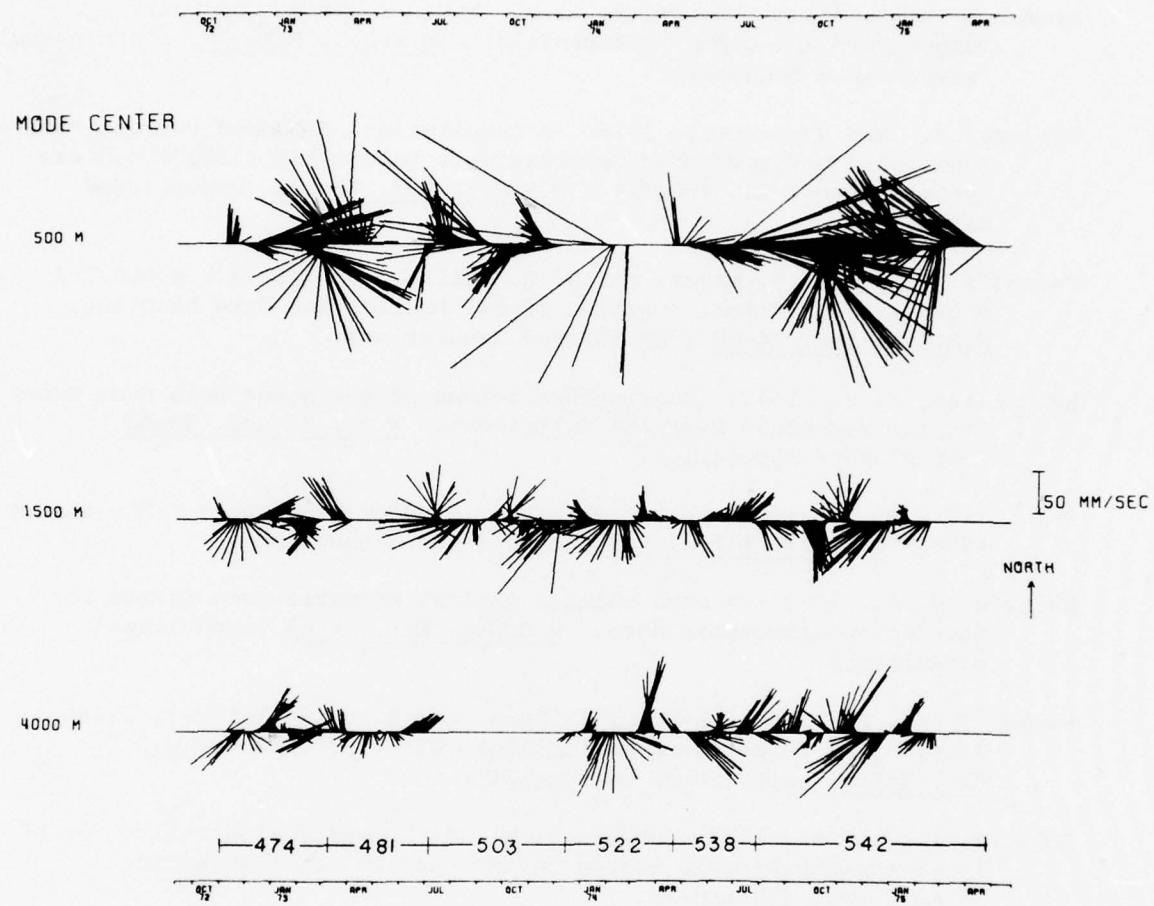
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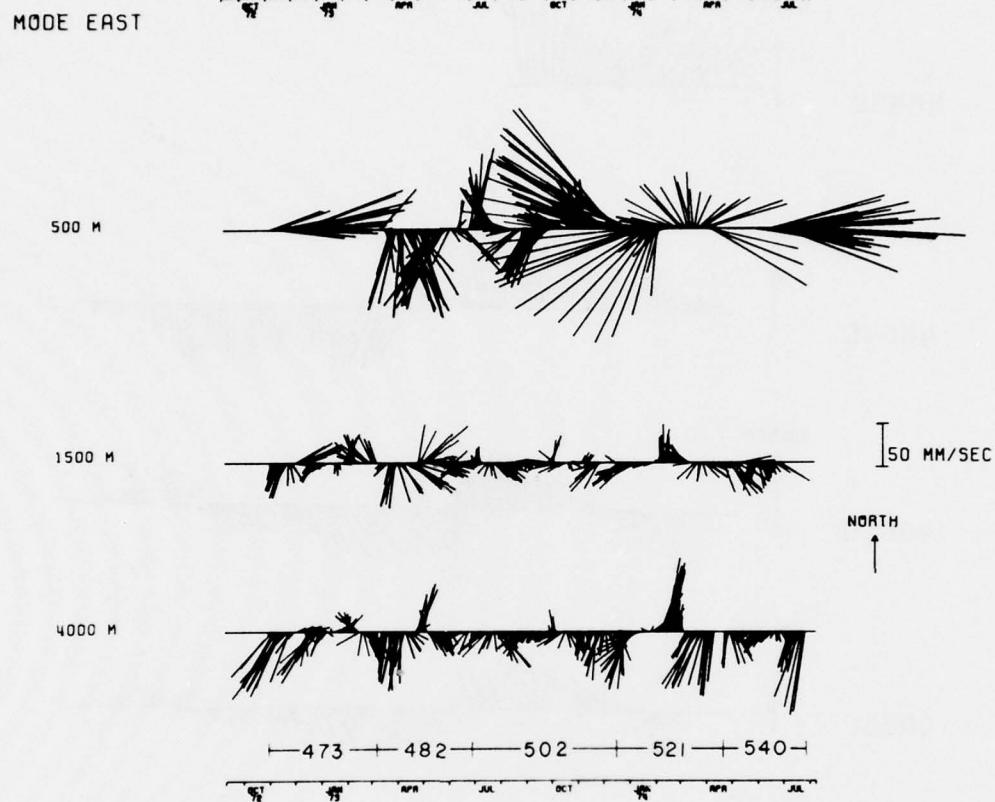
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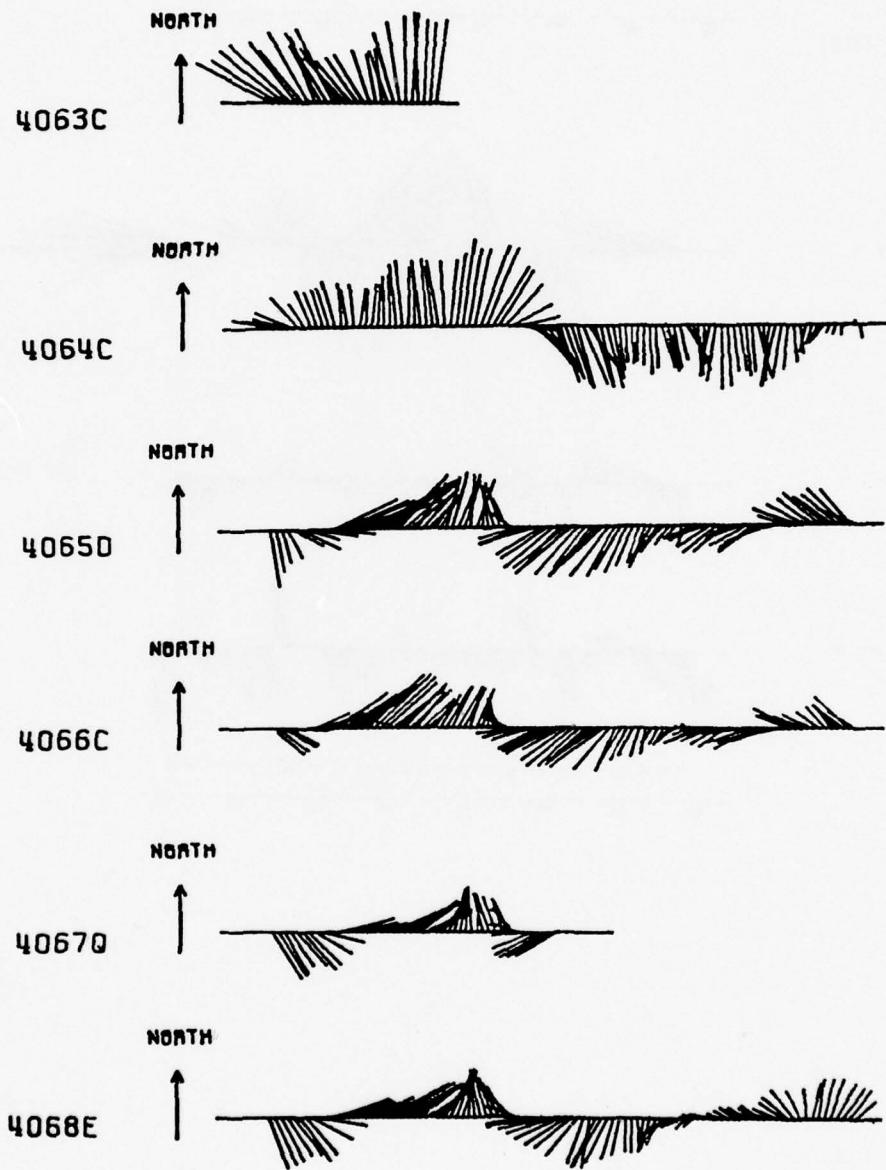
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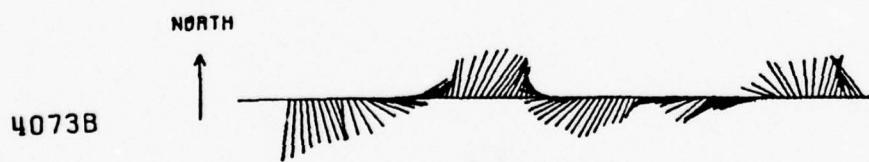
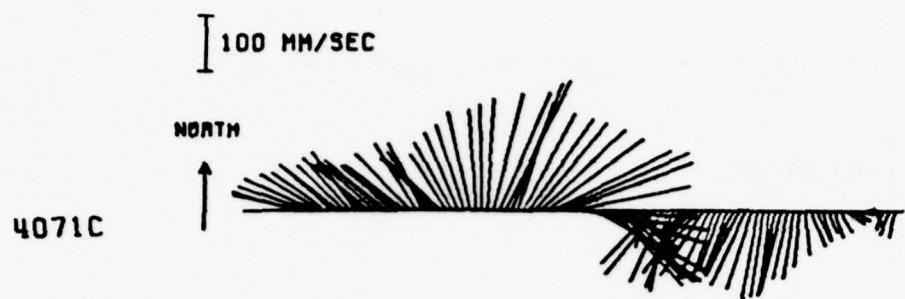


OCT '71 NOV DEC JAN '72 FEB

100 MM/SEC



OCT NOV DEC JAN FEB



OCT NOV DEC JAN FEB

FEB  
72

MAR

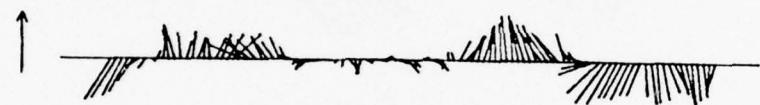
APR

MAY

100 MM/SEC

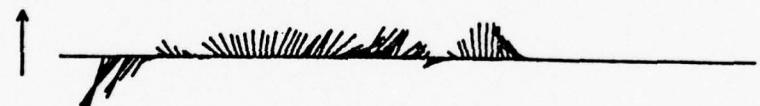
NORTH

4242J



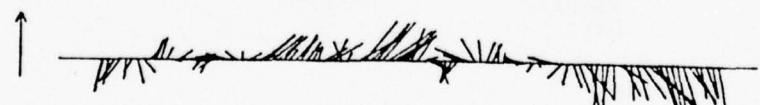
NORTH

4243D



NORTH

4244F



FEB  
72

MAR

APR

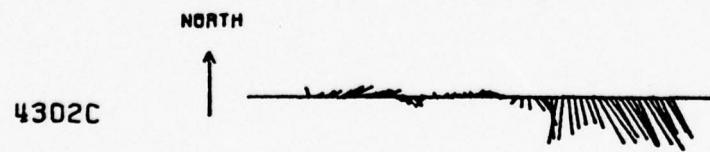
MAY

MAR  
72

APR

MAY

100 MM/SEC



MAR  
72

APR

MAY

MAY 72 JUN JUL AUG SEP OCT

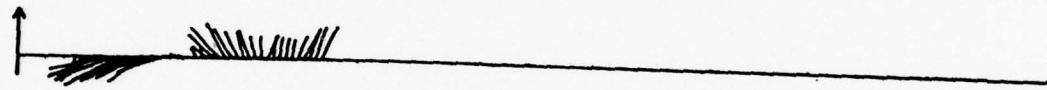
100 MM/SEC

4532A

NORTH

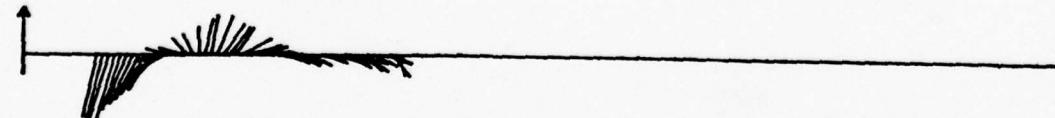


4533C



4536A

NORTH



MAY 72 JUN JUL AUG SEP OCT

1-C-7

MAY JUN JUL AUG SEP OCT

100 MM/SEC

NORTH

4552C



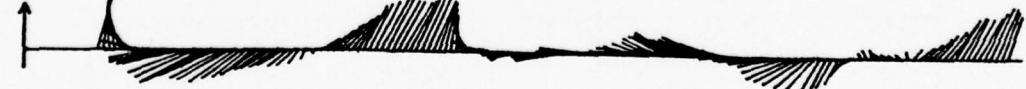
4553B

NORTH



4554H

NORTH



MAY JUN JUL AUG SEP OCT

1-C-8

ARRAY 1

1500 M.

XI-02	XI-04	XI-06	XI-08	XI-10
1 1 1	1 1 1	1 1 1	1 1 1	1 1 1
XI-12	XI-14	XI-16	XI-18	XI-20
1	1	1	1	1
1 1 1	1 1 1	1 1 1	1 1 1	1 1 1
XI-22	XI-24	XI-26	XI-28	XI-30
1	1	1	1	1
1 1 1	1 1 1	1 1 1	1 1 1	1 1 1
XII-02	XII-04	XII-06	XII-08	XII-10
1	1	1	1	1
1 1 1	1 1 1	1 1 1	1 1 1	1 1 1
XII-12	XII-14	XII-16	XII-18	XII-20
1	1	1	1	1
1 1 1	1 1 1	1 1 1	1 1 1	1 1 1
XII-22	XII-24	XII-26	XII-28	XII-30
1	1	1	1	1
1 1 1	1 1 1	1 1 1	1 1 1	1 1 1
I-01	I-03	I-05	I-07	I-09
1	1	1	1	1
1 1 1	1 1 1	1 1 1	1 1 1	1 1 1
I-11	I-13	I-15	I-17	I-19
1	1	1	1	1
1 1 1	1 1 1	1 1 1	1 1 1	1 1 1
I-21	I-23	I-25	I-27	I-29
1	1	1	1	1
1 1 1	1 1 1	1 1 1	1 1 1	1 1 1
I-31	II-02	II-04	II-06	
1 1 1	1 1 1	1 1 1	1 1 1	
				410
				407 409 412
				408 △ 406 411

0 200 0 200  
KM MM/SEC

1-D-1

XI - 02	XI - 04	XI - 06
$\Delta .30 \Delta .46$ 4.48	$\Delta .34 \Delta .45$ 4.48	$\Delta .37 \Delta .46$ 4.48
XI - 08	XI - 10	XI - 12
$\Delta .36 \Delta .45$ 4.46	$\Delta .36 \Delta .46$ 4.45	$\Delta .38 \Delta .46$ 4.47
XI - 14	XI - 16	XI - 18
$\Delta .38 \Delta .46$ 4.44	$\Delta .32 \Delta .46$ 4.43	$\Delta .32 \Delta .46$ 4.44
XI - 20	XI - 22	XI - 24
$\Delta .30 \Delta .46$ 4.42	$\Delta .28 \Delta .46$ 4.41	$\Delta .33 \Delta .41$ 4.42
XI - 26	XI - 28	XI - 30
$\Delta .32 \Delta .42$ 4.43	$\Delta .36 \Delta .41$ 4.41	$\Delta .35 \Delta .44$ 4.40
XII - 02	XII - 04	XII - 06
$\Delta .35 \Delta .41$ 4.42	$\Delta .31 \Delta .38$ 4.41	$\Delta .20 \Delta .42$ 4.40
XII - 08	XII - 10	XII - 12
$\Delta .18 \Delta .44$ 4.43	$\Delta .19 \Delta .45$ 4.39	$\Delta .22 \Delta .43$ 4.32
XII - 14	XII - 16	XII - 18
$\Delta .31 \Delta .38$ 4.40	$\Delta .35 \Delta .38$ 4.42	$\Delta .35 \Delta .33$ 4.41
XII - 20	XII - 22	XII - 24
$\Delta .31 \Delta .28$ 4.35	$\Delta .29 \Delta .32$ 4.38	$\Delta .33 \Delta .33$ 4.30
XII - 26	XII - 28	XII - 30
$\Delta .27 \Delta .28$ 4.27	$\Delta .23 \Delta .25$ 4.24	$\Delta .23 \Delta .28$ 4.22
I - 01	I - 03	I - 05
$\Delta .18 \Delta .26$ 4.21	$\Delta .18 \Delta .26$ 4.24	$\Delta .18 \Delta .23$ 4.21
I - 07	I - 09	I - 11
$\Delta .20 \Delta .27$ 4.24	$\Delta .20 \Delta .24$ 4.25	$\Delta .21 \Delta .25$ 4.23
I - 13	I - 15	I - 17
$\Delta .21 \Delta .26$ 4.17	$\Delta .22 \Delta .23$ 4.20	$\Delta .23 \Delta .20$ 4.25
I - 19	I - 21	I - 23
$\Delta .19 \Delta .24$ 4.21	$\Delta .19 \Delta .24$ 4.21	$\Delta .18 \Delta .22$ 4.17
I - 25	I - 27	I - 29
$\Delta .18 \Delta .22$ 4.18	$\Delta .21 \Delta .23$ 4.21	$\Delta .21 \Delta .26$ 4.23
I - 31	II - 02	II - 04
$\Delta .19 \Delta .25$ 4.25	$\Delta .22 \Delta .27$ 4.24	$\Delta .21 \Delta .26$ 4.23
II - 06	407 $\Delta$ 406 $\Delta$ 412 409 $\Delta$ $\Delta$ $\Delta$	

0 20  
KM

TEMPERATURE IN DEGREES C

## ARRAY 1

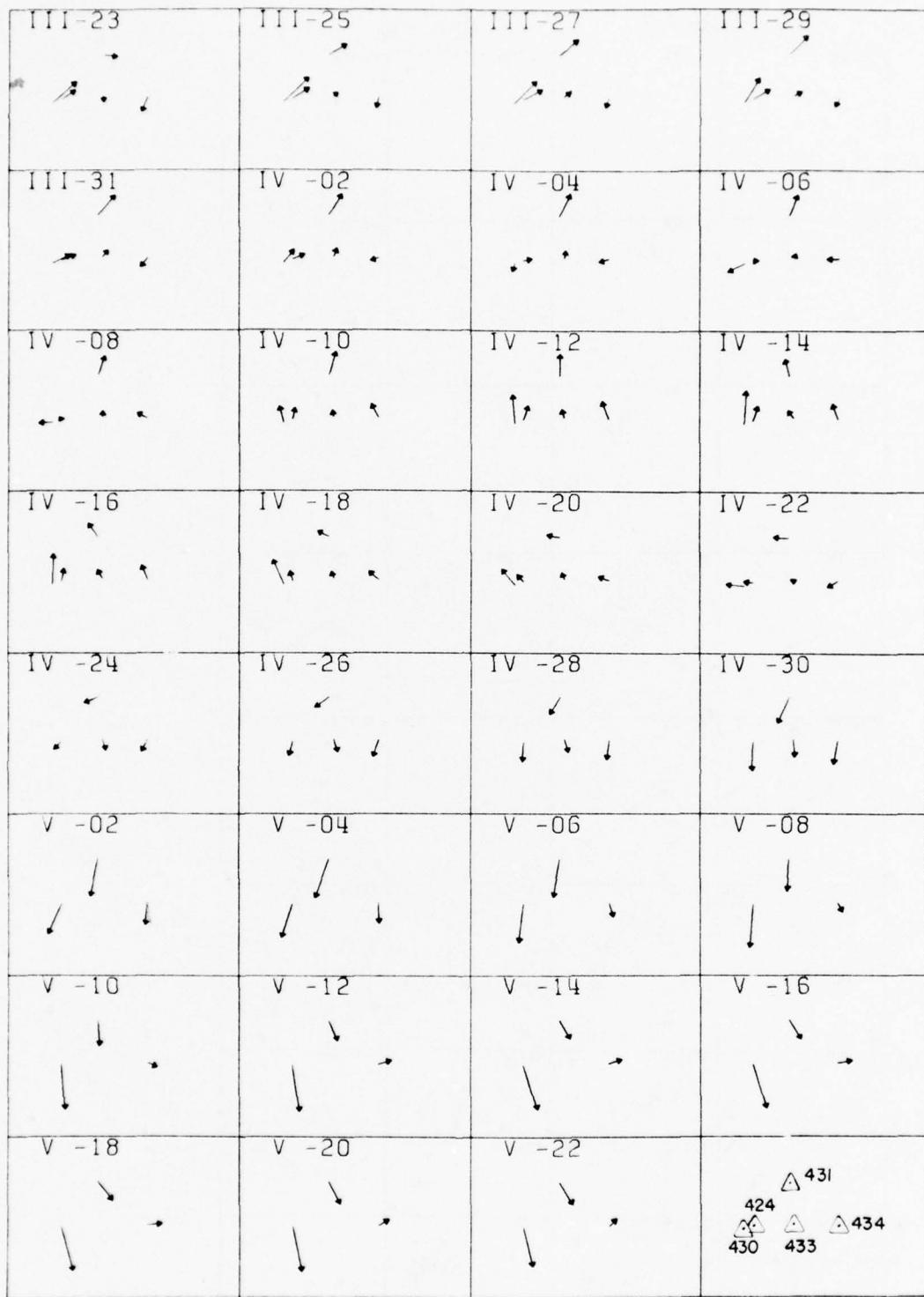
4000 M.

XI-03	XI-05	XI-07	XI-09	XI-11
1 11	1 11	1 11	1 11	1 11
XI-13	XI-15	XI-17	XI-19	XI-21
1 11	1 11	1 11	1 11	1 11
XI-23	XI-25	XI-27	XI-29	XI-31
1 11	1 11	1 11	1 11	1 11
XII-03	XII-05	XII-07	XII-09	XII-11
1 11	1 11	1 11	1 11	1 11
XII-13	XII-15	XII-17	XII-19	XII-21
1 11	1 11	1 11	1 11	1 11
XII-23	XII-25	XII-27	XII-29	XII-31
1 11	1 11	1 11	1 11	1 11
I-02	I-04	I-06	I-08	I-10
1	1	1	1	1
1 1	1 1	1 1	1 1	1 1
I-12	I-14	I-16	I-18	I-20
1	1	1	1	1
1 1	1 1	1 1	1 1	1 1
I-22	I-24	I-26	I-28	I-30
1	1	1	1	1
1 1	1 1	1 1	1 1	1 1
II-01	II-03	II-05	II-07	II-09
1	1	1	1	1
1 1	1 1	1 1	1 1	1 1
				410
				409
				407
				406

0 20 0 200  
KM MM/SEC

## ARRAY 2

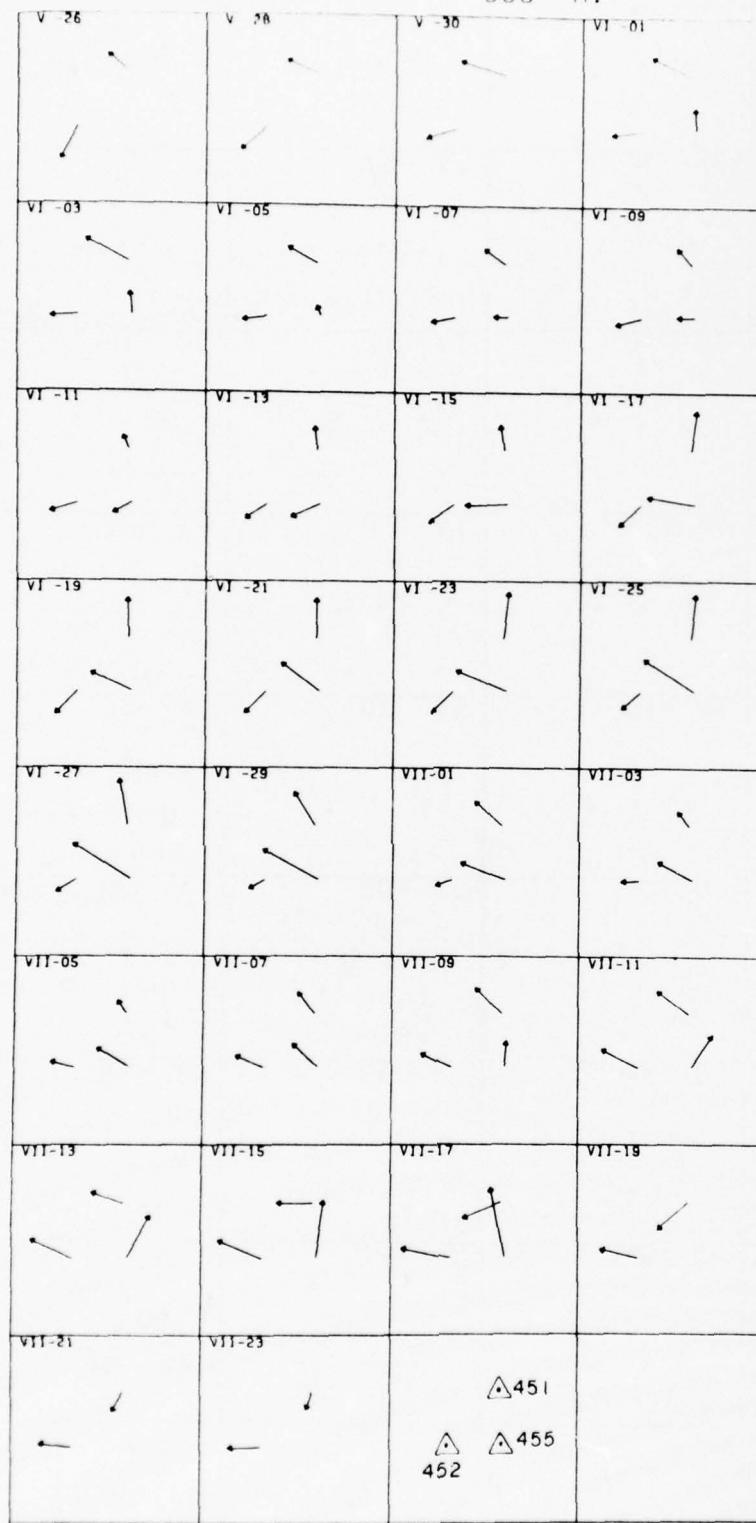
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0 20 0 200  
KM MM/SEC

## ARRAY 3

500 M.



0 20 0 200  
KM MM/SEC

## ARRAY 3

500 M.

V -26 Δ <sup>16.19</sup> Δ <sup>16.29</sup>	V -28 Δ <sup>16.08</sup> Δ <sup>16.27</sup>	V -30 Δ <sup>16.00</sup> Δ <sup>16.22</sup> Δ <sup>15.84</sup>	VI -01 Δ <sup>15.83</sup> Δ <sup>16.16</sup> Δ <sup>16.02</sup> Δ <sup>15.90</sup>
VI -03 Δ <sup>15.76</sup> Δ <sup>16.12</sup> Δ <sup>16.09</sup> Δ <sup>15.95</sup>	VI -05 Δ <sup>15.74</sup> Δ <sup>16.10</sup> Δ <sup>16.08</sup> Δ <sup>15.96</sup>	VI -07 Δ <sup>15.72</sup> Δ <sup>16.10</sup> Δ <sup>16.07</sup> Δ <sup>15.99</sup>	VI -09 Δ <sup>15.74</sup> Δ <sup>16.12</sup> Δ <sup>16.13</sup> Δ <sup>16.00</sup>
VI -11 Δ <sup>15.76</sup> Δ <sup>16.12</sup> Δ <sup>16.10</sup> Δ <sup>16.16</sup>	VI -13 Δ <sup>15.77</sup> Δ <sup>16.11</sup> Δ <sup>16.06</sup> Δ <sup>16.23</sup>	VI -15 Δ <sup>15.79</sup> Δ <sup>16.08</sup> Δ <sup>16.02</sup> Δ <sup>16.17</sup>	VI -17 Δ <sup>15.79</sup> Δ <sup>16.12</sup> Δ <sup>15.98</sup> Δ <sup>16.13</sup>
VI -19 Δ <sup>15.76</sup> Δ <sup>16.13</sup> Δ <sup>15.94</sup> Δ <sup>16.12</sup>	VI -21 Δ <sup>15.81</sup> Δ <sup>16.14</sup> Δ <sup>15.98</sup> Δ <sup>16.11</sup>	VI -23 Δ <sup>15.88</sup> Δ <sup>16.15</sup> Δ <sup>16.02</sup> Δ <sup>16.19</sup>	VI -25 Δ <sup>15.89</sup> Δ <sup>16.18</sup> Δ <sup>16.07</sup> Δ <sup>16.26</sup>
VI -27 Δ <sup>15.98</sup> Δ <sup>16.19</sup> Δ <sup>16.12</sup> Δ <sup>16.33</sup>	VI -29 Δ <sup>15.98</sup> Δ <sup>16.19</sup> Δ <sup>16.22</sup> Δ <sup>16.34</sup>	VII-01 Δ <sup>15.95</sup> Δ <sup>16.16</sup> Δ <sup>16.16</sup> Δ <sup>16.39</sup>	VII-03 Δ <sup>15.96</sup> Δ <sup>16.10</sup> Δ <sup>16.15</sup> Δ <sup>16.47</sup>
VII-05 Δ <sup>16.01</sup> Δ <sup>16.06</sup> Δ <sup>16.12</sup> Δ <sup>16.52</sup>	VII-07 Δ <sup>16.08</sup> Δ <sup>16.02</sup> Δ <sup>16.08</sup> Δ <sup>16.49</sup>	VII-09 Δ <sup>16.16</sup> Δ <sup>16.01</sup> Δ <sup>16.09</sup> Δ <sup>16.42</sup>	VII-11 Δ <sup>16.24</sup> Δ <sup>16.00</sup> Δ <sup>16.15</sup> Δ <sup>16.42</sup>
VII-13 Δ <sup>16.29</sup> Δ <sup>15.99</sup> Δ <sup>16.19</sup> Δ <sup>16.49</sup>	VII-15 Δ <sup>16.26</sup> Δ <sup>15.97</sup> Δ <sup>16.28</sup> Δ <sup>16.54</sup>	VII-17 Δ <sup>16.22</sup> Δ <sup>15.92</sup> Δ <sup>16.31</sup> Δ <sup>16.69</sup>	VII-19 Δ <sup>16.15</sup> Δ <sup>15.90</sup> Δ <sup>16.71</sup>
VII-21 Δ <sup>16.11</sup> Δ <sup>15.91</sup> Δ <sup>16.68</sup>	VII-23 Δ <sup>16.13</sup> Δ <sup>15.86</sup> Δ <sup>16.75</sup>	Δ 451 Δ 452 Δ 455 Δ 453	

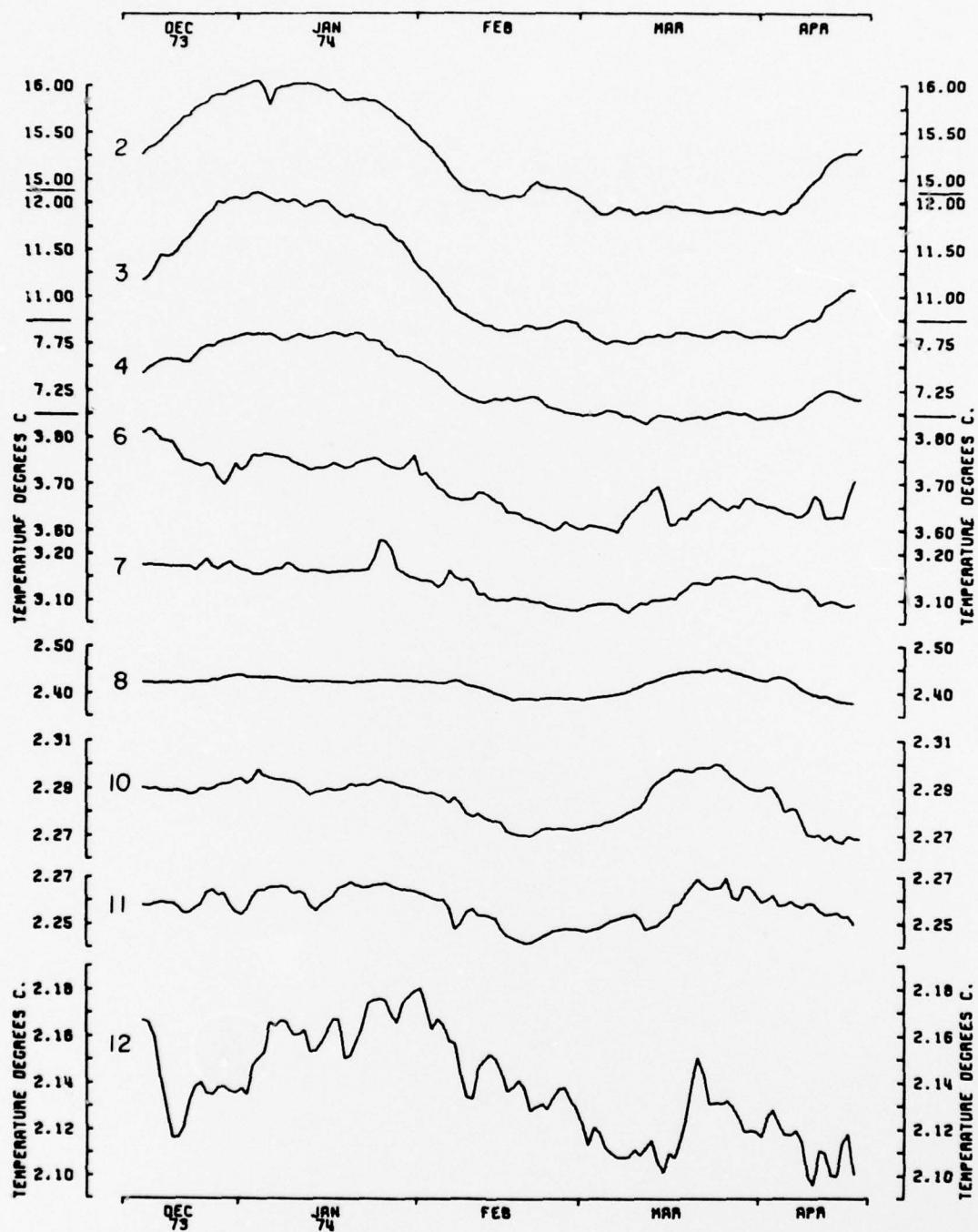
0 20  
KM  
TEMPERATURE IN DEGREES C

ARRAY 3

4000 m

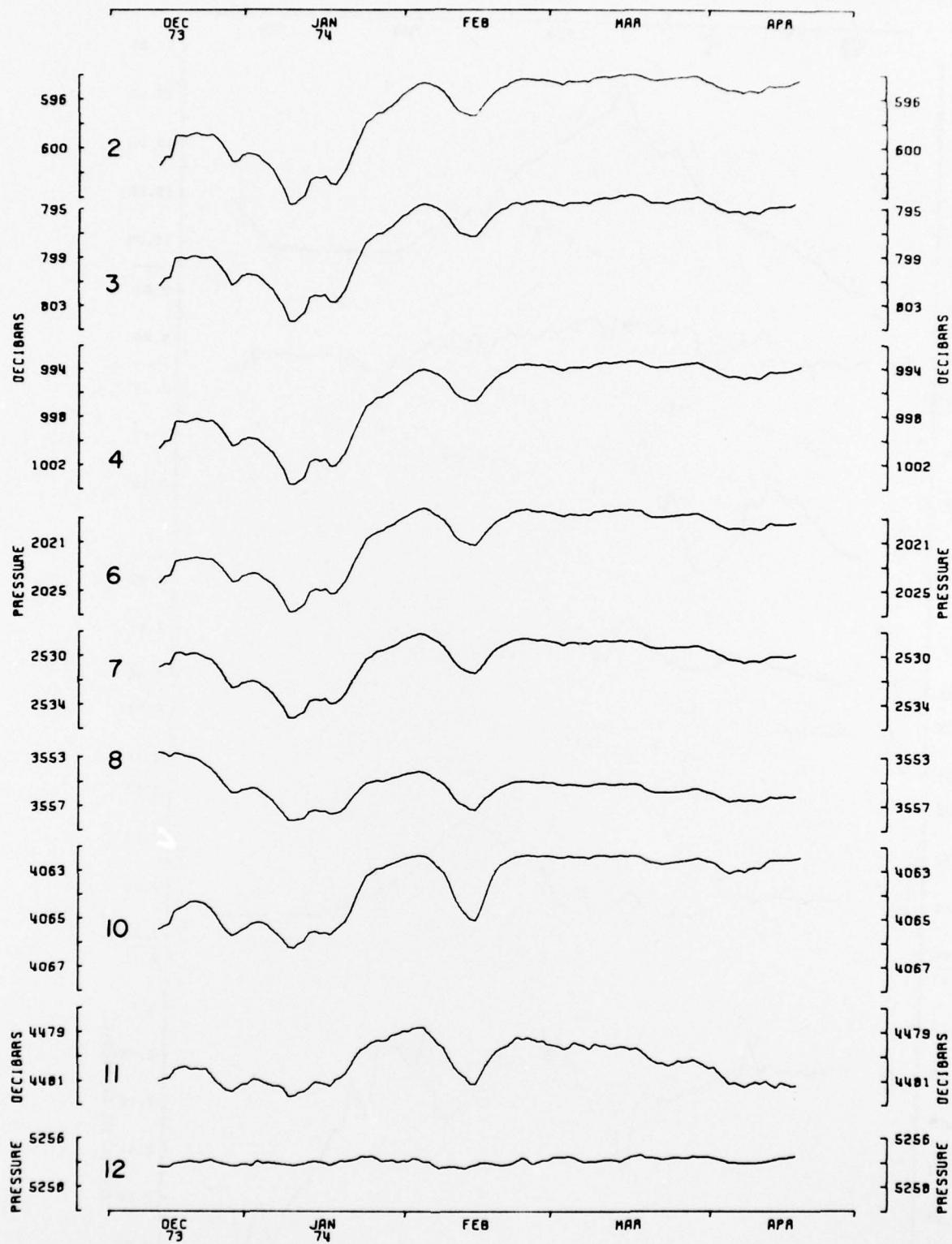
0  $200$   $200$   
KM MM/SEC

521



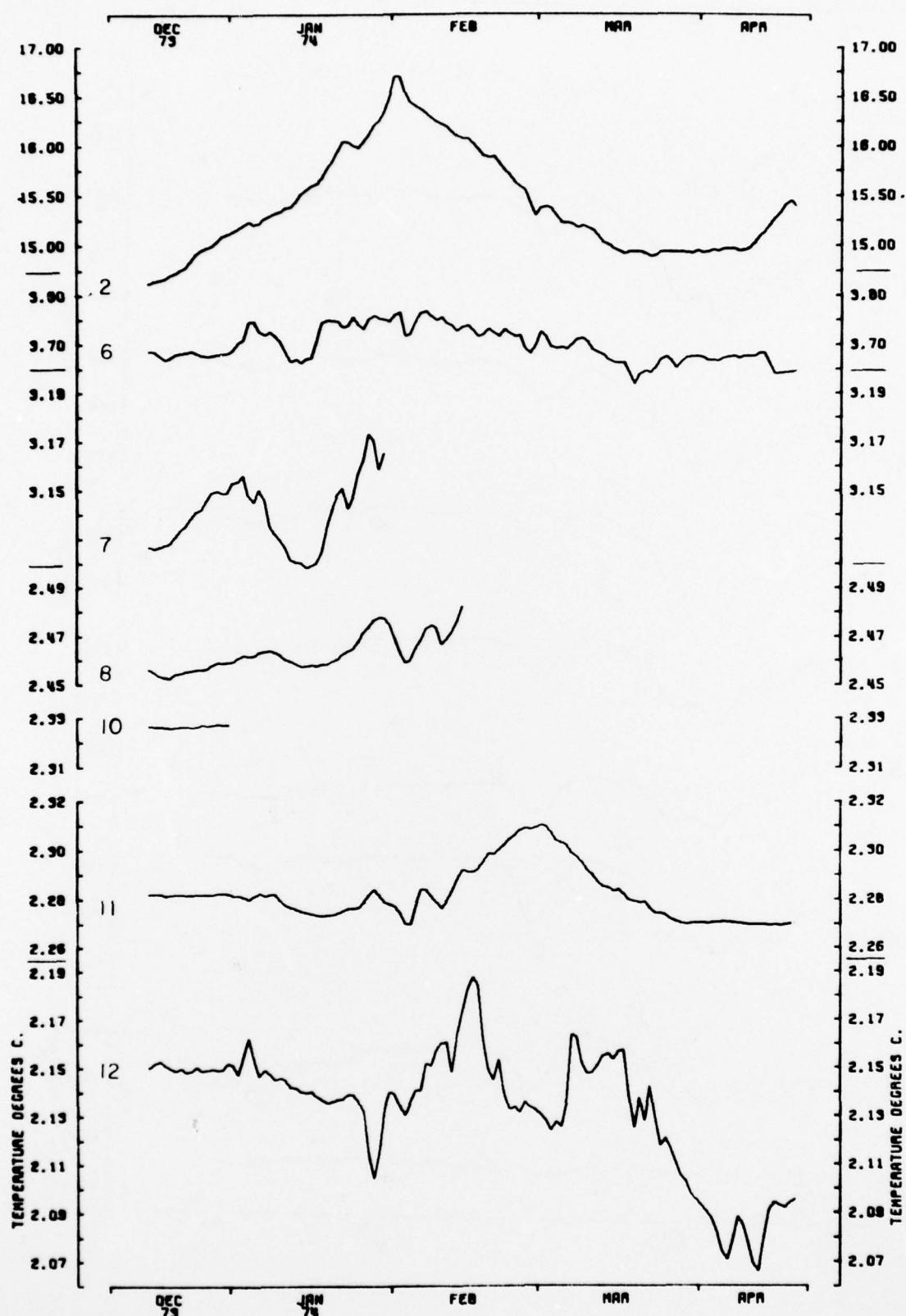
1-E-1

521



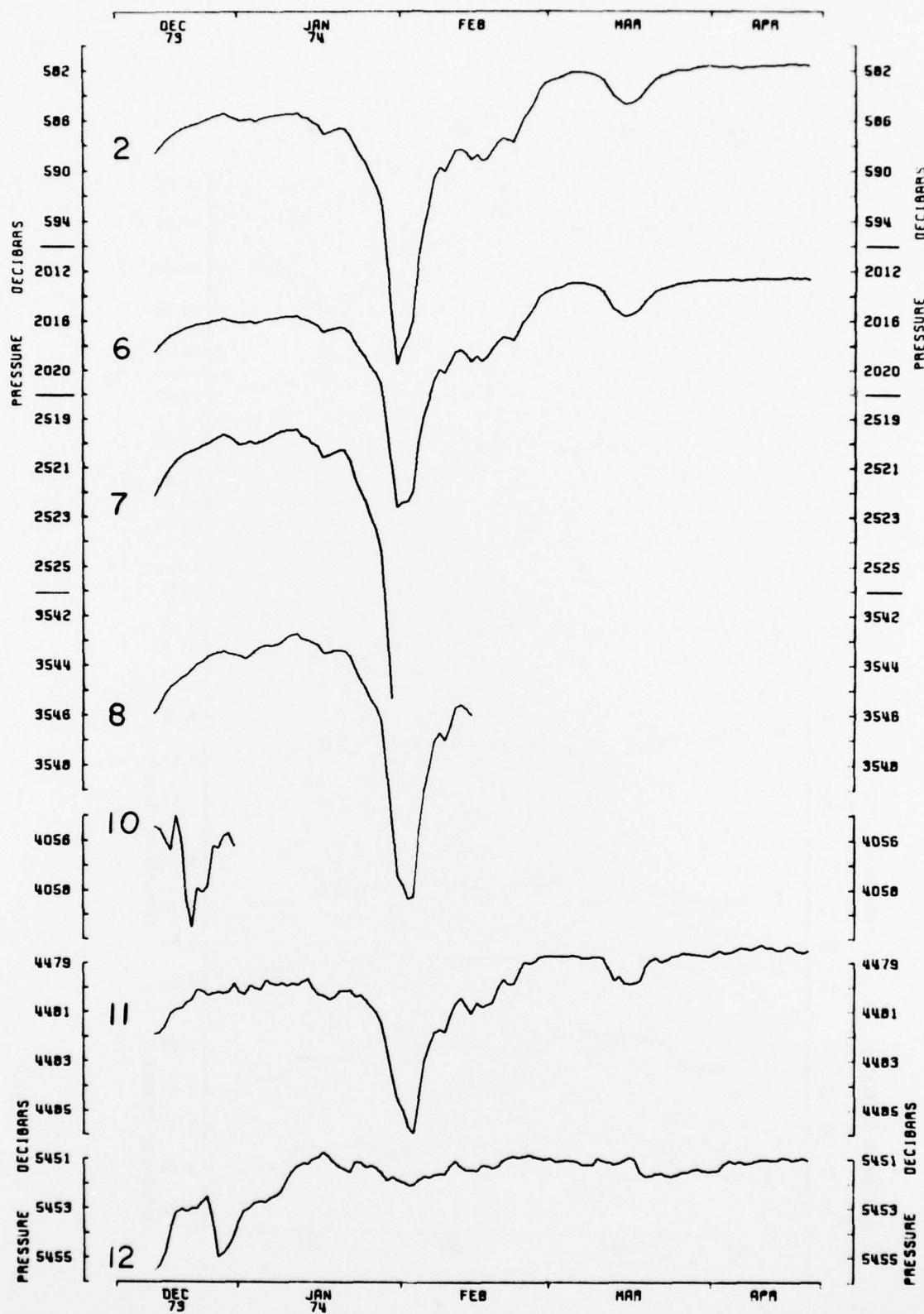
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522

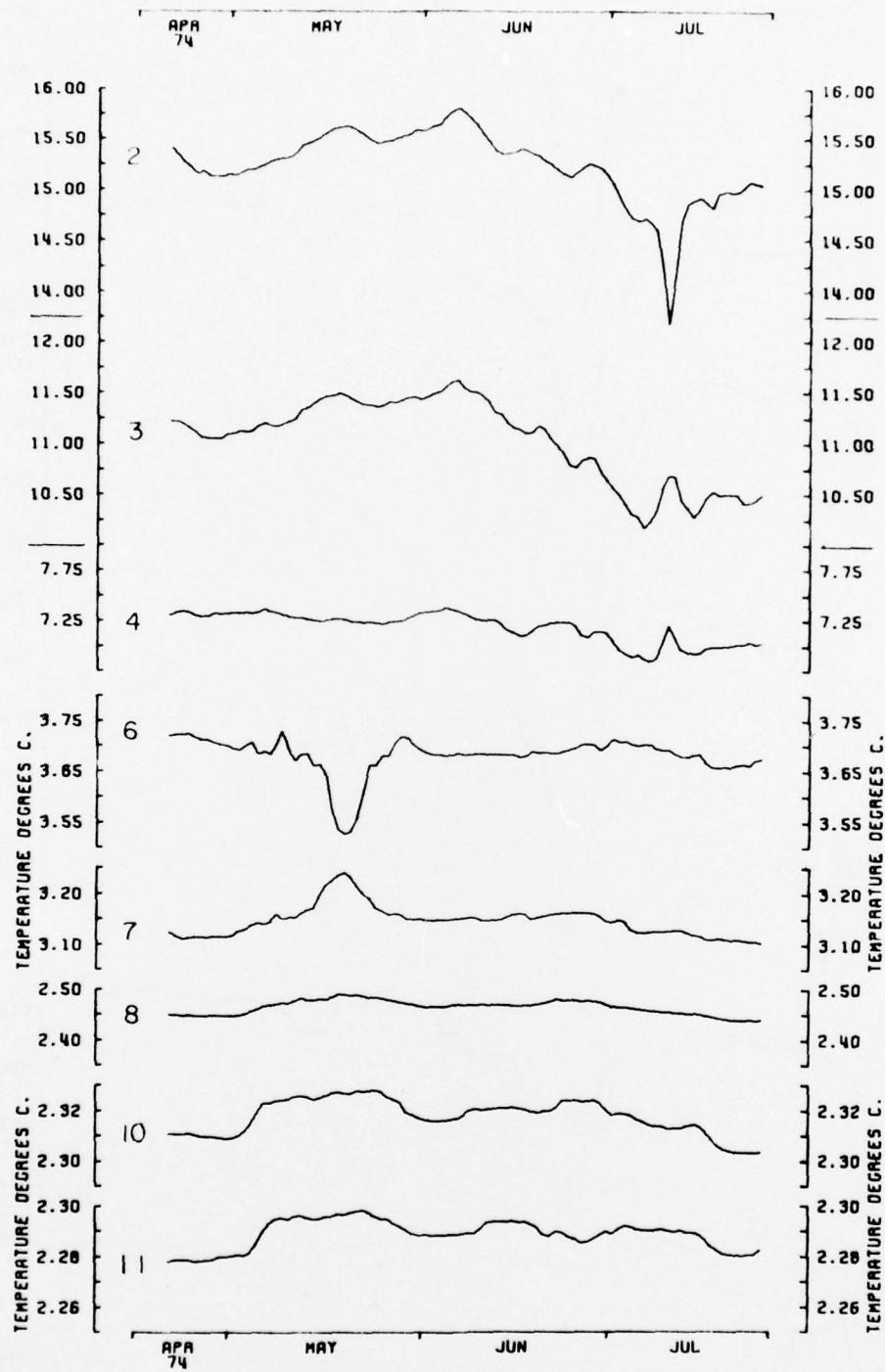


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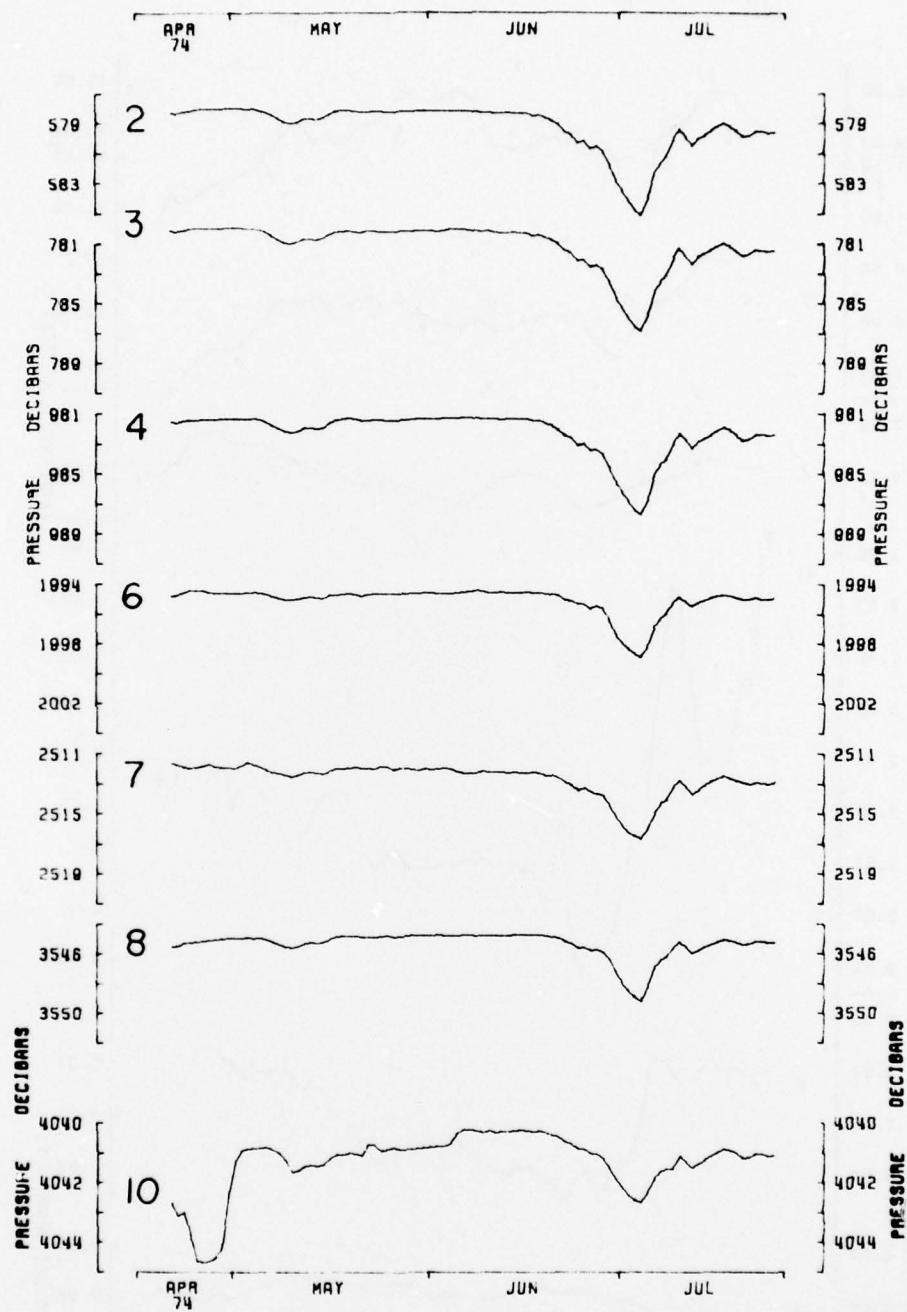


538



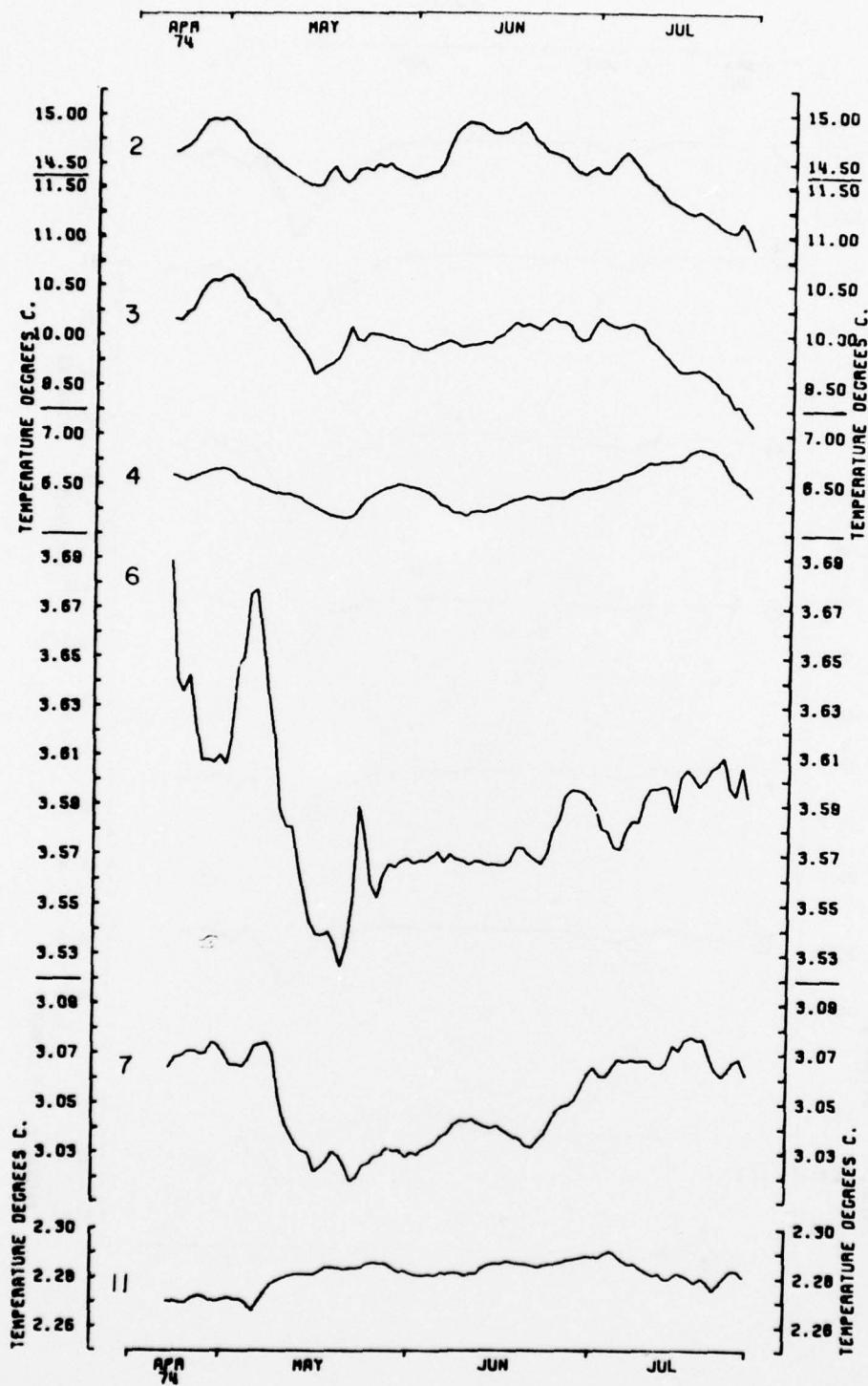
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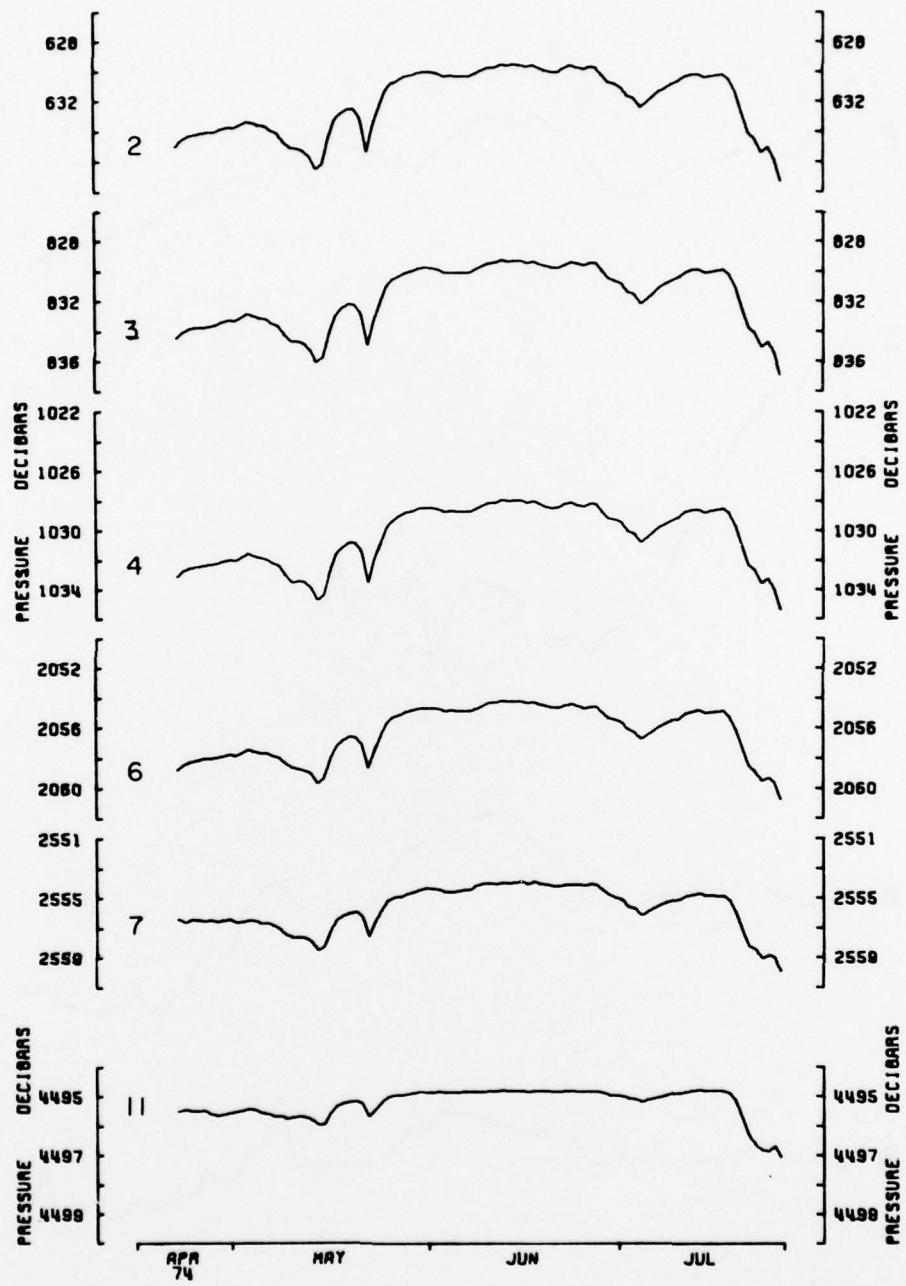
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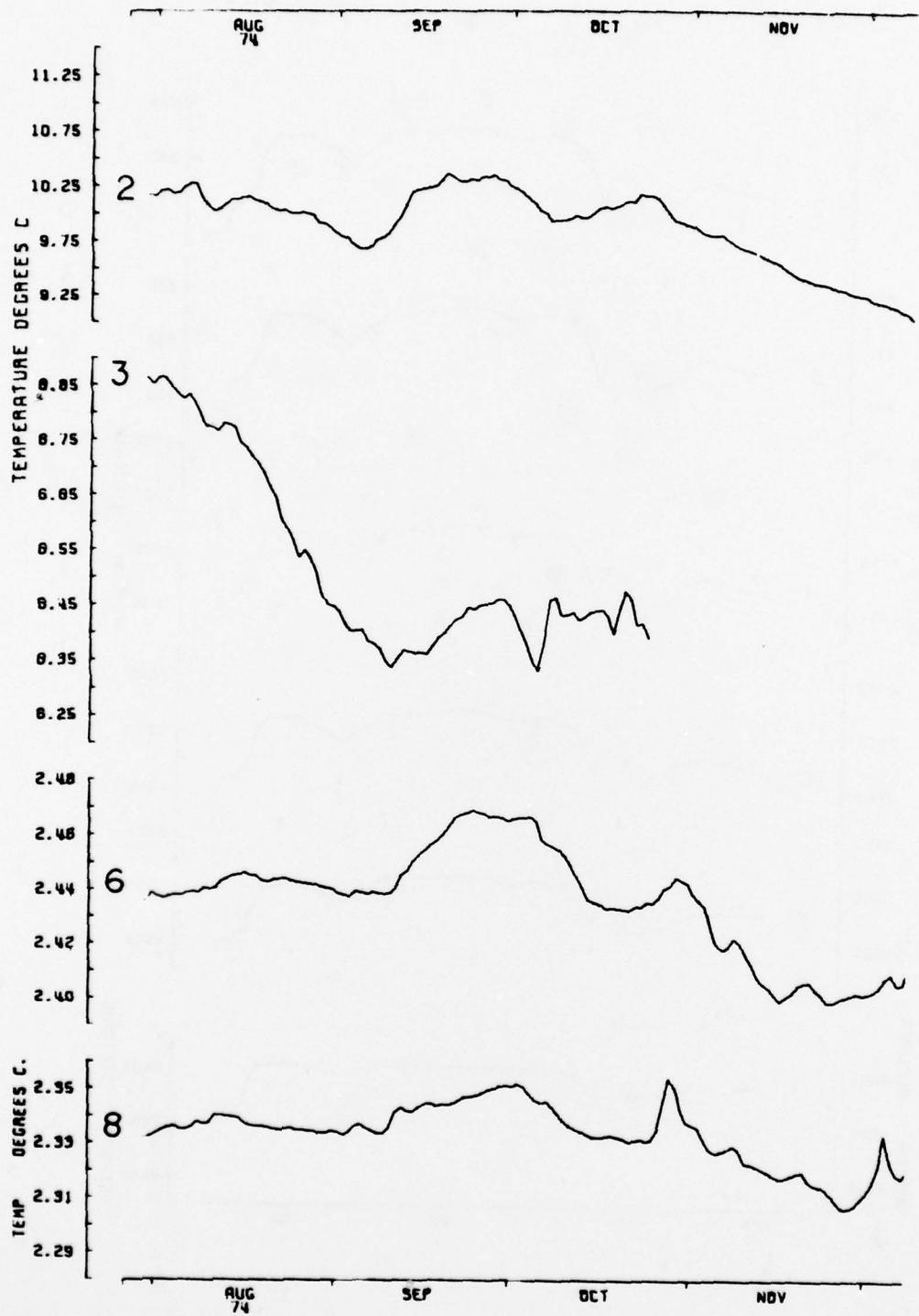
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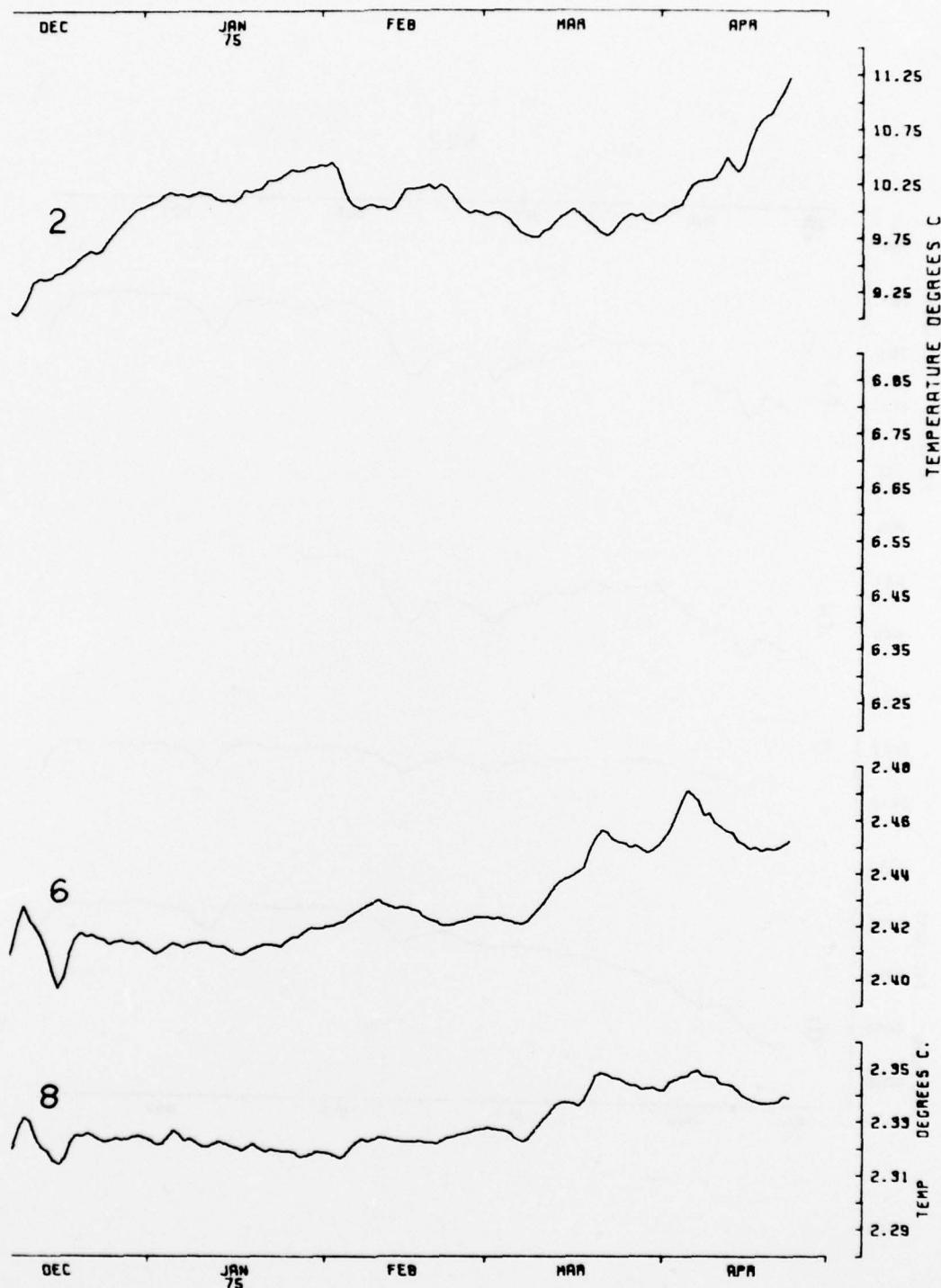
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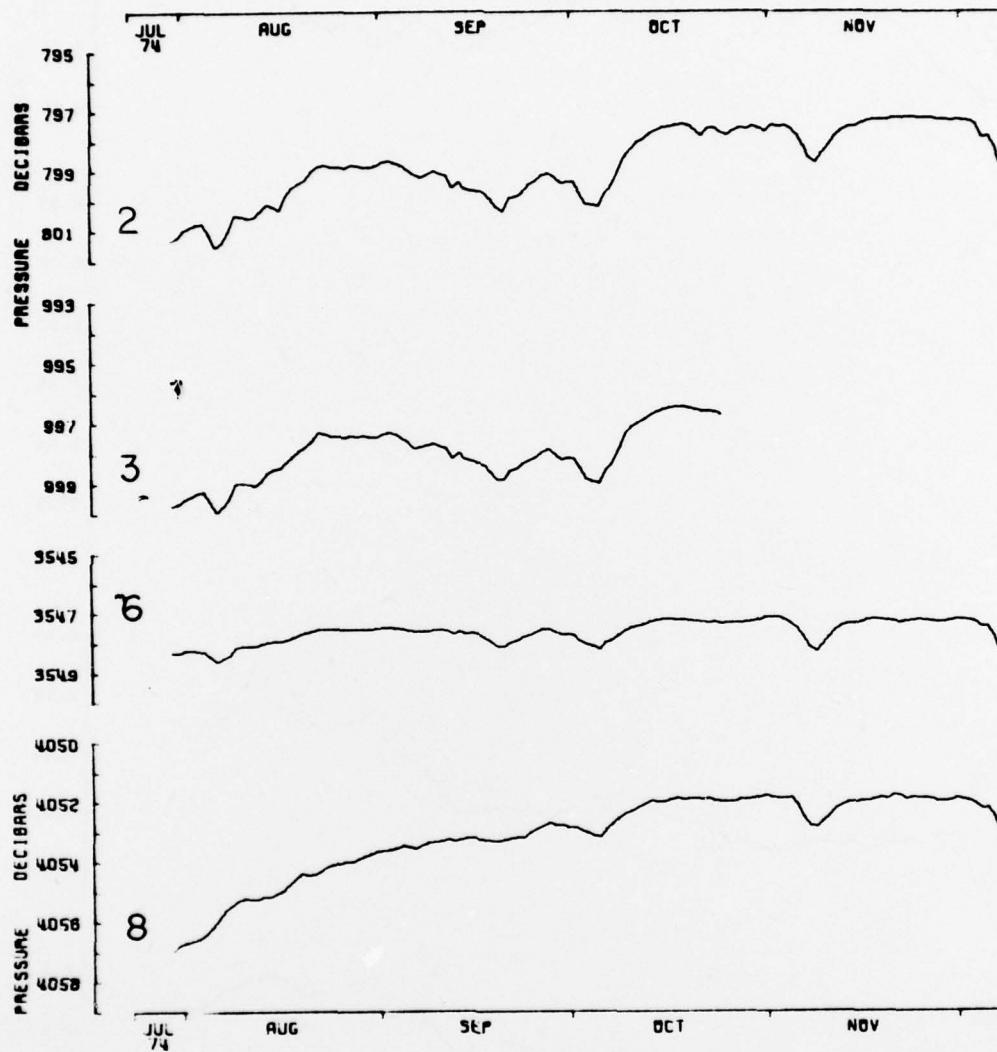
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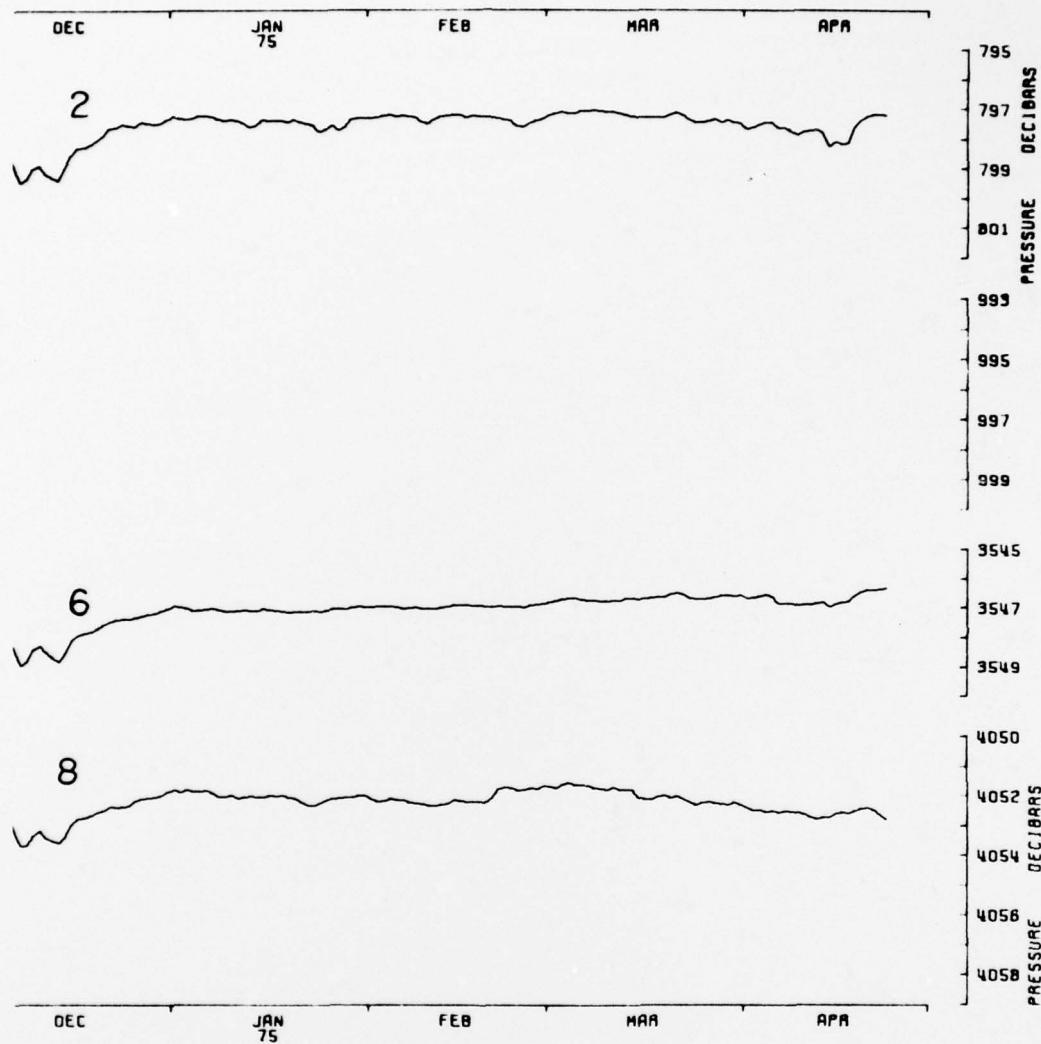
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Current, temperature and pressure measurements from instruments moored in the MODE area during the years 1971-1975 are presented. Record lengths vary from 2 weeks to 7 months. Data from individual instruments are displayed in the form of statistical tables, spectral plots and variables vs. time plots. Current data are additionally displayed as progressive vector plots. Composite plots of temperature, pressure or velocity are included for groups of records which could be combined to show a meaningful spatial or temporal array. Selected CTD data are included and displayed as potential temperature and salinity versus pressure.

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